GENERAL NAVIGATION

| 4090 | 61 | In a remote indicating compass system the amount of deviation caused by aircraft magnetism and electrical circuits may be minimised by: | positioning the master unit in the centre of the aircraft | using a vertically mounted gyroscope | mounting the detector unit in the wingtip | the use of repeater cards | 0 | 0 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4091 | 61 | (For this question use annex 061-12401A) <br> What are the average magnetic course and distance between | $\begin{array}{rc} 091^{\circ} & - \\ 562 & \mathrm{NM} \end{array}$ | $\begin{array}{rr} 105^{\circ} & - \\ 480 \mathrm{NM} \end{array}$ | $\begin{array}{r} 105^{\circ}- \\ 562 \mathrm{NM} \end{array}$ | $\begin{array}{rc} 091^{\circ} & - \\ 480 \mathrm{NM} \end{array}$ | 0 | 0 | 1 | 0 |
| 4092 | 61 | When decelerating on a westerly heading in the Northern hemisphere, the compass card of a direct reading magnetic compass will turn : | anti-clockwise giving an apparent tum towards the north | clockwise giving an apparent tum toward the south | anti-clockwise giving an apparent tum towards the south | clockwise giving an apparent tum towards the north | 0 | 1 | 0 | 0 |
| 4093 | 61 | The value of magnetic variation: | must be $0^{\circ}$ at the magnetic equator | varies between a maximum of $45^{\circ}$ East and $45^{\circ}$ West | cannot exceed $90^{\circ}$ | has a maximum of $180^{\circ}$ | 0 | 0 | 0 | 1 |
| 4094 | 61 | (For this question use annex 061-2304A) <br> The UTC of sunrise on 6 Decemberat WINNIPEG (Canada) | 0930 | 0113 | 2230 | 1413 | 0 | 0 | 0 | 1 |
| 4095 | 61 | (For this question use annexes 061-2305A and 061-2305B) <br> When it is 1000 Standard Time in Kuwait, the Standard Time in Algeria is: | 1200 | 1300 | 0700 | 0800 | 0 | 0 | 0 | 1 |
| 4096 | 61 | The north and south magnetic poles are the only positions on the earth's surface where: | the value of magnetic variation equals $90^{\circ}$ | a freely suspended compass needle will stand vertical | isogonals converge | a freely suspended compass needle will stand horizontal | 0 | 1 | 0 | 0 |
| 4097 | 61 | (For this question use annex 061-12400A) <br> What are the average magnetic course and distance between <br>  | $\begin{array}{rc} 118^{\circ} & - \\ 440 & \mathrm{NM} \end{array}$ | $\begin{array}{r} 117^{\circ}- \\ 494 \mathrm{NM} \end{array}$ | $\begin{array}{rc} 130^{\circ} & - \\ 440 & \mathrm{NM} \end{array}$ | $\begin{array}{rr} \hline 131^{\circ} & - \\ 494 \mathrm{NM} \end{array}$ | 0 | 0 | 0 | 1 |
| 4098 | 61 | On a Direct Mercator, rhumb lines are: | ellipses | curves convex to the equator | straight lines | curves concave to the equator | 0 | 0 | 1 | 0 |
| 4099 | 61 | What is the value of the convergence factor on a Polar Stereographic chart? | 0.866 | 0.5 | 0.0 | 1.0 | 0 | 0 | 0 | 1 |
| 4100 | 61 | Which one of the following describes the appearance of rhumb lines, except meridians, on a Polar Stereographic chart? | Ellipses around the Pole | Curves convex to the Pole | Straight lines | Curves concave to the Pole | 0 | 0 | 0 | 1 |
| 4101 | 61 | Which one of the following statements is correct concerning the appearance of great circles, with the exception of meridians, on a Polar Stereographic chart whose tangency is at the pole? | They are complex curves that can be convex and/or concave to the Pole | They are curves convex to the Pole | The higher the latitude the closer they approximate to a straight line | Any straight line is a great circle | 0 | 0 | 1 | 0 |
| 4102 | 61 | On a Lambert conformal conic chart, the distance between parallels of latitude spaced the same number of degrees apart : | expands between, and reduces outside, the standard parallels | is constant throughout the chart | reduces between, and expands outside, the standard parallels | is constant between, and expands outside, the standard parallels | 0 | 0 | 1 | 0 |


| 4103 | 61 | Which one of the following, concerning great circles on a Direct Mercator chart, is correct? | They are all curves concave to the equator | They approximate to straight lines between the standard parallels | They are all curves convex to the equator | With the exception of meridians and the equator, they are curves concave to the equator | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4104 | 61 | Parallels of latitude on a Direct Mercator chart are: | parallel straight lines equally spaced | arcs of concentric circles equally spaced | straight lines converging above the pole | parallel straight lines unequally spaced | 0 | 0 | 0 | 1 |
| 4105 | 61 | On a Direct Mercator chart, meridians are: | parallel, equally spaced, vertical straight lines | inclined, equally spaced, straight lines that meet at the nearer pole | parallel, unequally spaced, vertical straight lines | inclined, unequally spaced, curved lines that meet at the nearer pole | 1 | 0 | 0 | 0 |
| 4106 | 61 | Which is the highest latitude listed below at which the sun will rise above the horizon and set every day? | $66^{\circ}$ | $68^{\circ}$ | $72^{\circ}$ | $62^{\circ}$ | 1 | 0 | 0 | 0 |
| 4107 | 61 | The angle between Magnetic North and Compass North is called: | compass deviation | compass error | magnetic variation | alignment error | 1 | 0 | 0 | 0 |
| 4108 | 61 | A straight line on a Lambert Conformal Projection chart for normalflight planning purposes: | is <br> approximatel <br> y a Great <br> Circle | is a Loxodromic line | is a Rhumb line | can only be a parallel of latitude | 1 | 0 | 0 | 0 |
| 4109 | 61 | A Rhumb line is : | a line convex to the nearest pole on a Mercator proj ection | a line on the surface of the earth cutting all meridians at the same angle | the shortest distance between two points on a Polyconic projection | any straight line on a Lambert projection | 0 | 1 | 0 | 0 |
| 4110 | 61 | Contour lines on aeronautical maps and charts connect points: | having the same elevation above sea level | with the same variatio n | having the same longitude | of equal latitude | 1 | 0 | 0 | 0 |
| 4111 | 61 | (For this question use annex 061-1828A and the dat a for 1215 UTC) <br> 1215 UTC LAJES VORTAC ( $38^{\circ} 46^{\prime} \mathrm{N} 027^{\circ} 05^{\prime} \mathrm{W}$ ) RMI reads $178^{\circ}$, | $\begin{aligned} & 41^{\circ} 00^{\prime} \mathrm{N} \\ & 028^{\circ} 10^{\prime} \mathrm{W} \end{aligned}$ | $\begin{aligned} & 41^{\circ} 05^{\prime} \mathrm{N} \\ & 027^{\circ} 50^{\prime} \mathrm{W} \end{aligned}$ | $\begin{aligned} & 40^{\circ} 55^{\prime} \mathrm{N} \\ & 027^{\circ} 55^{\prime} \mathrm{W} \end{aligned}$ | $\begin{aligned} & 40^{\circ} 50^{\prime} \mathrm{N} \\ & 027^{\circ} 40^{\prime} \mathrm{W} \end{aligned}$ | 0 | 0 | 1 | 0 |
| 4112 | 61 | A chart has the scale 1:1000000. From A to B on the chart measures 1.5 inches (one inch equals 2.54 centimetres), the distance from $A$ to $B$ in NM is : | 20.6 | 38.1 | 44.5 | 54.2 | 1 | 0 | 0 | 0 |
| 4113 | 61 | The angle between the plane of the ecliptic and the plane of equator is approximately : | $23.5^{\circ}$ | $25.3^{\circ}$ | $27.5^{\circ}$ | $66.5^{\circ}$ | 1 | 0 | 0 | 0 |
| 4114 | 61 | A ground feature appears $30^{\circ}$ to the left of the centre line of the CRT of an airborne weather radar. If the heading of the aircraft is $355^{\circ}(\mathrm{M})$ and the magnetic variation is $15^{\circ}$ East, the true bearing of the aircraft from the feature is: | $310^{\circ}$ | $130^{\circ}$ | $160^{\circ}$ | $220^{\circ}$ | 0 | 0 | 10 | 0 |
| 4115 | 61 | On which of the following chart projections is it NOT possible to represent the north or south poles? | Transverse Mercator | Polar stereographi C | Direct <br> Mercator | Lambert's conformal | 0 | 0 | 10 | 0 |
| 4116 | 61 | The chart distance between meridians $10^{\circ}$ apart at latitude $65^{\circ}$ North is 3.75 inches. The chart scale at this latitude approximates: | 1:6000 000 | 1:2500 000 | 1:3000 000 | 1:5000 000 | 0 | 0 | 0 | 1 |


| 4117 | 61 | (For this question use annex 061-1818A) <br> Assume a North polar stereographic chart whose grid is aligned with the Greenwich meridian. <br> An aircraft flies from the geographic North pole for a distance of 480 NM along the $110^{\circ} \mathrm{E}$ meridian, then follows a grid track | $\begin{aligned} & 70^{\circ} 15^{\prime \prime} \mathrm{N} \\ & 080^{\circ} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 80^{\circ} 00^{\prime} \mathrm{N} \\ & 080^{\circ} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 78^{\circ} 45^{\prime} \mathrm{N} \\ & 087^{\circ} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 79^{\circ} 15^{\prime} \mathrm{N} \\ & 074^{\circ} \mathrm{E} \end{aligned}$ | 0 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4118 | 61 | Some inertial reference and navigation systems are known as "strapdown". <br> This means that: | only the gyros, and not the acceleromete rs, become part of the unit's fixture to the aircraft struct ure | gyros and acceleromete rs are mounted on a stabilised platform in the aircraft | gyros and acceleromete rs need sat ellite information input to obtain a vertical reference | the <br> gyroscopes and acceleromete rs become part of the unit's fixture to the aircraft struct ure | 0 | 0 | 0 |
| 4119 | 61 | As the INS position of the departure aerodrome, coordinates $35^{\circ} 32.7^{\prime} \mathrm{N} 139^{\circ} 46.3^{\prime} \mathrm{W}$ are input instead of $35^{\circ} 32.7^{\prime} \mathrm{N}$ $139^{\circ} 46.3^{\prime} \mathrm{E}$. When the aircraft subsequently passes point $52^{\circ} \mathrm{N} 180^{\circ} \mathrm{W}$, the longitude value shown on the INS will be: | 080 ${ }^{\circ} 27.4^{\prime} \mathrm{W}$ | 099³2.6'W | 099 ${ }^{\circ} 32.6^{\prime} \mathrm{E}$ | 080 ${ }^{\circ} 27.4{ }^{\prime} \mathrm{E}$ | 0 | 1 | 00 |
| 4120 | 61 | In order to maintain an accurate vertical using a pendulous system, an aircraft inertial platform incorporates a device: | without damping and a period of 84.4SEC | with damping and a period of 84.4 SEC | with damping and a period of 84.4 MIN | without damping and a period of 84.4 MIN | 0 | - | 10 |
| 4121 | 61 | On a Transverse Mercator chart, scale is exactly correct along the: | meridian of tangency | Equator, parallel of origin and prime vertical | datum meridian and meridian perpendicula $r$ to it | prime meridian and the equator | 1 | 0 | 00 |
| 4122 | 61 | On a Lambert Conformal Conic chart earth convergency is most accurately represented at the: | parallel of origin | north and south limits of the chart | standard parallels | Equator | 1 | 0 | 0 |
| 4123 | 61 | The total length of the $53^{\circ} \mathrm{N}$ parallel of latitude on a direct Mercator chart is 133 cm . What is the approximate scale of the chart at latitude $30^{\circ} \mathrm{S}$ ? | $\begin{aligned} & 1: 30000 \\ & 000 \end{aligned}$ | $\begin{aligned} & 1: 18000 \\ & 000 \end{aligned}$ | $\begin{aligned} & 1: 21000 \\ & 000 \end{aligned}$ | $\begin{aligned} & 1: 25000 \\ & 000 \end{aligned}$ | 0 | 0 | 0 |
| 4124 | 61 | What is the chart distance between longitudes $179^{\circ} \mathrm{E}$ and $175^{\circ} \mathrm{W}$ on a direct Mercator chart with a scale of $1: 5000$ 000 at the equator? | 167 mm | 72 mm | 133 mm | 106 mm | 0 | 0 | 10 |
| 4125 | 61 | The constant of the cone, on a Lambert chart where the convergence angle between longitudes $010^{\circ} \mathrm{E}$ and $030^{\circ} \mathrm{W}$ is $30^{\circ}$, is: | 0.50 | 0.64 | 0.75 | 0.40 | 0 | 0 | 10 |
| 4126 | 61 | The platform of an inertial navigation system (INS) is maintained at right angles to the local vertical by applying corrections for the effects of: | gyroscopic inertia, earth rotation and real drift | vertical velocities, earth precession, centrifugal forces and transport drift | movement in the yawing plane, secondary precession and pendulous oscillation | aircraft manoeuvres, earth rotation, transport wander and coriolis | 0 | 0 | 0 |
| 4127 | 61 | (For this question use annex 061-2326A to 061-2326D) <br> When it is 0600 Standard Time in Queensland (Australia) the Standard Time in Hawaii (USA) is: | 0200 | 0600 | 1000 | 1200 | 0 | 0 | 10 |
| 4128 | 61 | (For this question use annex 061-2325A to 061-2325D) <br> An aircraft takes off from Guam at 2300 Standard Time on 30 April local date. <br> After a flight of 11 HR 15 MIN it lands at Los Angeles (California). | $\begin{aligned} & 1715 \text { on } 30 \\ & \text { April } \end{aligned}$ | $\begin{aligned} & 1215 \text { on } 1 \\ & \text { May } \end{aligned}$ | $\begin{aligned} & 1315 \text { on } 1 \\ & \text { May } \end{aligned}$ | $\begin{aligned} & 1615 \text { on } 30 \\ & \text { April } \end{aligned}$ |  | 0 | 0 |


| 4129 | 61 | Isogonals converge at the: | Magnetic equator | North magnetic pole only | North and South magnetic poles only | North and South geographic and magnetic pol es | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4130 | 61 | When accelerating on an easterly heading in the Northem hemisphere, the compass card of a direct reading magnetic compass will turn : | anti-clockwise giving an apparent tum toward the south | clockwise giving an apparent tum toward the north | clockwise giving an apparent tum toward the south | anti-clockwise giving an apparent tum toward the north | 0 | 1 | 0 | 0 |
| 4131 | 61 | When tuming right from $330^{\circ}(\mathrm{C})$ to $040^{\circ}(\mathrm{C})$ in the northern hemisphere, the reading of a direct reading magnetic compass will: | over-indicate the tum and liquid swirl will decrease the effect | under-indicat e the turn and liquid swirl will decrease the effect | over-indicate the tum and liquid swirl will increase the effect | under-indicat e the turn and liquid swirl will increase the effect | 0 | 0 | 0 | 1 |
| 4132 | 61 | An aircraft in the northern hemisphere makes an accurate rate one turn to the right/starboard. If the initial heading was $330^{\circ}$, after 30 seconds of the turn the direct reading magnetic compass should read: | 060 ${ }^{\circ}$ | $\begin{aligned} & \text { more than } \\ & 060^{\circ} \end{aligned}$ | more or less than $060^{\circ}$ depending on the pendulous suspension used | $\left\lvert\, \begin{aligned} & \text { less than } \\ & 060^{\circ} \end{aligned}\right.$ | 0 | 0 | 0 | 1 |
| 4133 | 61 | The horizontal component of the earth's magnetic field: | weakens with increasing distance from the magnetic poles | weakens with increasing distance from the nearer magnetic pole | is <br> approximatel <br> $y$ the same at all magnetic latitudes less than $60^{\circ}$ | is <br> approximatel $y$ the same at magnetic latitudes $50^{\circ} \mathrm{N}$ and $50^{\circ} \mathrm{S}$ | 0 |  | 0 | 1 |
| 4134 | 61 | A line drawn on a chart which joins all points where the value of magnetic variation is zero is called an: | agonic line | aclinic line | isogonal | isotach | 1 | 0 | 0 | 0 |
| 4135 | 61 | A Lambert conformal conic projection, with two standard parallels: | shows lines of longitude as parallel straight lines | the scale is only correct along the standard parallels | shows all great circles as straight lines | the scale is only correct at parallel of origin | 0 | 1-1 | 1-1 | 0 |
| 4136 | 61 | On a Lambert Conformal chart the distance between meridians $5^{\circ}$ apart along latitude $37^{\circ}$ North is 9 cm . The scale of the chart at that parallel approximates: | 1:2000 000 | 1:6000 000 | 1:5000 000 | 1:3750000 | 0 | 0 | 1 | 0 |
| 4137 | 61 | On the 27 th of February, at $52^{\circ} \mathrm{S}$ and $040^{\circ} \mathrm{E}$, the sunrise is at 0243 UTC. <br> On the same day, at $52^{\circ} \mathrm{S}$ and $035^{\circ} \mathrm{W}$, the sunrise is at: | 0523 UTC | 0743 UTC | 0243 UTC | 2143 UTC | 0 | 1 | 0 | 0 |
| 4138 | 61 | An aeroplane flies from $\mathrm{A}\left(59^{\circ} \mathrm{S} 142^{\circ} \mathrm{W}\right)$ to $\mathrm{B}\left(61^{\circ} \mathrm{S} 148^{\circ} \mathrm{W}\right)$ with a TAS of 480 kt . <br> The autopilot is engaged and coupled with an Inertial Navigation System in which AB track is active. | varies by $10^{\circ}$ | decreases by $6^{\circ}$ | varies by $4^{\circ}$ | increases by $5^{\circ}$ | 0 | 0 | 0 | 1 |
| 4139 | 61 | The rhumb-line distance between points $\mathrm{A}\left(60^{\circ} 00^{\prime} \mathrm{N}\right.$ $002^{\circ} 30^{\prime} \mathrm{E}$ ) and $\mathrm{B}\left(60^{\circ} 00^{\prime} \mathrm{N} 007^{\circ} 30^{\prime} \mathrm{W}\right)$ is: | 300 NM | 450 NM | 600 NM | 150 NM | 1 | 0 | 0 | 0 |
| 4140 | 61 | An aircraft is over position $\mathrm{HO}\left(55^{\circ} 30^{\prime} \mathrm{N} 060^{\circ} 15^{\prime} \mathrm{W}\right)$, where YYR VOR ( $53^{\circ} 30^{\prime} \mathrm{N} 060^{\circ} 15 \mathrm{~W}$ ) can be received. The magnetic variation is $31^{\circ} \mathrm{W}$ at HO and $28^{\circ} \mathrm{W}$ at YYR . <br> What is the radialfrom YYR? | $031^{\circ}$ | $332^{\circ}$ | 028 ${ }^{\circ}$ | $208^{\circ}$ | 0 | 0 | 1 | 0 |
| 4141 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=485 \mathrm{kt} \\ & \mathrm{OAT}=\mathrm{ISA}+10^{\circ} \mathrm{C} \end{aligned}$ | 0.87 | 0.825 | 0.90 | 0.85 | 0 | 1 | 0 | 0 |


| 4142 | 61 | Given: <br> A polar stereographic chart whose grid is aligned with the zero meridian. <br> Grid track $344^{\circ}$, | 099 | $1279^{\circ}$ | 049 | $1229^{\circ}$ | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4143 | 61 | For a distance of 1860 NM between $Q$ and $R$, a ground speed "out" of 385 kt , a ground speed "back" of 465 kt and an endurance of 8 HR (excluding reserves) the distance from $Q$ to the point of safe retum (PSR) is: | 1685 NM | 1532 NM | 930 NM | 1865 NM | 1 | 0 | 0 | 0 |
| 4144 | 61 | An aircraft travels from point A to point B, using the autopilot connected to the aircraft's inertial system. The coordinates of $\mathrm{A}\left(45^{\circ} \mathrm{S} 010^{\circ} \mathrm{W}\right)$ and $\mathrm{B}\left(45^{\circ} \mathrm{S} 030^{\circ} \mathrm{W}\right)$ have been entered. <br> The true course of the aircraft on its arrival at $B$, to the nearest degree, is: | $277^{\circ}$ | $284{ }^{\circ}$ | $263^{\circ}$ | $270^{\circ}$ | 1 | 0 | 0 | 0 |
| 4145 | 61 | The constant of cone of a Lambert conformal conic chart is quoted as 0.3955. <br> At what latitude on the chart is earth convergency correctly | 68 ${ }^{\circ} 25^{\prime}$ | 21 ${ }^{\circ} 35^{\prime}$ | 23¹8' | 66º ${ }^{\circ}$ ' | 0 | 0 | 1 | 0 |
| 4146 | 61 | The duration of civil twilight is the time: | agreed by the internatio nal aeronautical authorities which is 12 minutes | needed by the sun to move from the apparent height of $0^{\circ}$ to the apparent height of $6^{\circ}$ | between sunset and when the centre of the sun is $12^{\circ}$ below the true horizon | between sunset and when the centre of the sun is $6^{\circ}$ below the true horizon | 0 | 0 | 0 | 1 |
| 4147 | 61 | The Great Circle bearing of ' $\mathrm{B}^{\prime}\left(70^{\circ} \mathrm{S} 060^{\circ} \mathrm{E}\right)$, from ' $\mathrm{A}^{\prime}\left(70^{\circ} \mathrm{S}\right.$ $030^{\circ} \mathrm{W}$, is approximately: | $150^{\circ}(\mathrm{T})$ | 090 ${ }^{\circ}$ (T) | $315^{\circ}(\mathrm{T})$ | $135^{\circ}$ (T) | 0 | 0 | 0 | 1 |
| 4148 | 61 | In a navigation chart a distance of 49 NM is equal to 7 cm . The scale of the chart is approximately: | 1:7000 000 | 1:1300 000 | 1:700000 | 1:130000 | 0 | 1 | 0 | 0 |
| 4149 | 61 | At $60^{\circ} \mathrm{N}$ the scale of a direct Mercator chart is $1: 3000000$. <br> What is the scale at the equator? | 1:3000 000 | 1:3500 000 | 1:1500 000 | 1:6000 000 | 0 | 0 | 0 | 1 |
| 4150 | 61 | During initial alignment an inertial navigation system is north aligned by inputs from: | horizontal acceleromete rs and the east gyro | the aircraft remote reading compass system | computer matching of measured gravity magnitude to gravity magnitude of initial alignment | vertical acceleromete rs and the north gyro | 1 | 0 | 0 | 0 |
| 4151 | 61 | An aircraft is flying with the aid of an inertial navigation system (INS) connected to the autopilot. The following two points have been entered in the INS computer: <br> WPT 1: $60^{\circ} \mathrm{N} 030^{\circ} \mathrm{W}$ <br> WPT 2: $60^{\circ} \mathrm{N} 020^{\circ} \mathrm{W}$ <br> When $025^{\circ} \mathrm{W}$ is passed the latitude shown on the display unit of the inertial naviaation svstem will be: | $60^{\circ} 00.0^{\prime} \mathrm{N}$ | $59^{\circ} 49.0^{\prime} \mathrm{N}$ | $6^{\circ}{ }^{\circ} 11.0^{\prime} \mathrm{N}$ | $60^{\circ} 05.7^{\prime} \mathrm{N}$ | 0 | 0 | 0 | 1 |
| 4152 | 61 | The azimuth gyro of an inertial unit has a drift of $0.01^{\circ} / \mathrm{HR}$. After a flight of 12 HR with a ground speed of 500 kt , the error on the aeroplane position is approximately : | 6 NM | 60 NM | 12 NM | 1 NM | 0 | 0 | 1 | 0 |
| 4153 | 61 | The drift of the azimuth gyro on an inertial unit induces an error in the position given by this unit. "t" being the elapsed time. | proportional to t /2 | sinusoîdal | proportional to $t$ | proportional to the square of time, $\mathrm{t}^{2}$ | 0 | - | 1 | 0 |
| 4154 | 61 | With reference to inertial navigation systems, a TAS input is: | required to provide a W $/ V$ read out | not required | required for Polar navigation | required for rhumb line navigation | 1 | 0 | 0 | 0 |


$\square$

| 4155 | 61 | Given: $\begin{aligned} & \mathrm{AD}=\text { Air distance } \\ & \mathrm{GD}=\text { Ground distance } \\ & \text { TAS = True Airspeed } \end{aligned}$ | $\begin{aligned} & \text { GD = (AD X } \\ & \text { GS)/TAS } \end{aligned}$ | $\begin{aligned} & \mathrm{GD}=(\mathrm{AD}- \\ & \mathrm{TAS}) / \mathrm{TAS} \end{aligned}$ | $\begin{aligned} & \text { GD = AD X } \\ & \text { (GS } \\ & \text {-TAS)/GS } \end{aligned}$ | $\begin{aligned} & \text { GD }= \\ & \text { TAS/(GS X } \\ & \text { AD) } \end{aligned}$ | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4156 | 61 | (For this question use annex 061-12583A) <br> Given: <br> SHA VOR (N5243.3 W00853.1) radial $143^{\circ}$, | $\begin{aligned} & \hline \text { N5210 } \\ & \text { W00800 } \end{aligned}$ | $\begin{aligned} & \text { N5155 } \\ & \text { W00810 } \end{aligned}$ | $\begin{aligned} & \text { N5205 } \\ & \text { W00805 } \end{aligned}$ | $\begin{aligned} & \text { N5200 } \\ & \text { W00800 } \end{aligned}$ | 1 | 0 |
| 4157 | 61 | (For this question refer to annex 061-12604A) <br> What feature is shown on the chart at position N5211 | Connemara aerodrome | Punchestown aerodrome | KERRY/Farra nfore aerodrome | Waterford NDB | 0 | 0 |
| 4158 | 61 | (For this question use annex 061-12589A) <br> Given: <br> SHA VOR N5243.3 W00853.1 <br> CRK VORN5150.4 W00829.7 | $\begin{aligned} & \text { SHA } 205^{\circ} \\ & \text { CRK } 321^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA 033} \\ & \text { CRK } 149^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 212^{\circ} \\ & \text { CRK } 328^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 025^{\circ} \\ & \text { CRK } 141^{\circ} \end{aligned}$ | 0 | 0 |
| 4159 | 61 | (For this question use annex 061-12588A) <br> Given: <br> SHA VOR/DME (N5243.3 W00853.1) radial 048\%/22 NM. | $\begin{aligned} & \hline \text { N5228 } \\ & \text { W00920 } \end{aligned}$ | $\begin{aligned} & \text { N5300 } \\ & \text { W0830 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5258 } \\ & \text { W00825 } \end{aligned}$ | $\begin{aligned} & \text { N5225 } \\ & \text { W00917 } \end{aligned}$ | - | 1 |
| 4160 | 61 | (For this question use annex 061-12587A) <br> Given: <br> SHA VOR/DME (N5243.3 W00853.1) radial 025/49 NM. | $\begin{aligned} & \text { N5155 } \\ & \text { W00915 } \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { N5200 } \\ \text { W0925 } \end{array}$ | $\begin{aligned} & \text { N5330 } \\ & \text { W00830 } \end{aligned}$ | $\begin{aligned} & \text { N5328 } \\ & \text { W00820 } \end{aligned}$ | 0 | 0 |
| 4161 | 61 | (For this question use annex 061-12586A) <br> Given: <br> SHA VOR/DME (N5243.3 W00853.1) radial $232^{\circ} / 32$ NM. | $\begin{aligned} & \text { N5228 } \\ & \text { W00935 } \end{aligned}$ | $\begin{aligned} & \text { N5303 } \\ & \text { W00810 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5220 } \\ & \text { W00930 } \end{aligned}$ | $\begin{aligned} & \text { N5305 } \\ & \text { W00815 } \end{aligned}$ | 0 | 0 |
| 4162 | 61 | (For this question use annex 061-12591A) <br> Given: <br> SHA VOR N5243.3 W00853.1 <br> CRK VOR N5150.4 W00829.7 | $\begin{aligned} & \text { SHA 068} \\ & \text { CRK } 145^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 060^{\circ} \\ & \text { CRK } 138^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 240^{\circ} \\ & \text { CRK } 137^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 248^{\circ} \\ & \text { CRK } 325^{\circ} \end{aligned}$ | 0 | 0 |
| 4163 | 61 | (For this question use annex 061-12584A) <br> Given: <br> SHA VOR/DME (N5243.3 W00853.1) radial 120\%35 NM. | $\begin{aligned} & \text { N5250 } \\ & \text { W00950 } \end{aligned}$ | $\begin{aligned} & \text { N5230 } \\ & \text { W00800 } \end{aligned}$ | $\begin{aligned} & \text { N5300 } \\ & \text { W00945 } \end{aligned}$ | $\begin{aligned} & \text { N5225 } \\ & \text { W00805 } \end{aligned}$ | 0 | - |
| 4164 | 61 | (For this question use annex 061-12592A) <br> Given: <br> SHA VOR N5243.3 W00853.1 <br> CON VOR N5354.8 W00849.1 | $\begin{aligned} & \text { SHA 042} \\ & \text { CON } 138^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 213^{\circ} \\ & \operatorname{CON} 310^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA 033 } \\ & \text { CON } 130^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 221^{\circ} \\ & \operatorname{CON} 318^{\circ} \end{aligned}$ | 1 | 0 |
| 4165 | 61 | (For this question use annex 061-12582A) <br> Given: <br> SHA VOR (N5243.3 W00853.1) radial $129^{\circ}$, | $\begin{aligned} & \text { N5220 } \\ & \text { W00750 } \end{aligned}$ | $\begin{aligned} & \text { N5215 } \\ & \text { W00755 } \end{aligned}$ | $\begin{aligned} & \text { N52 10 } \\ & \text { W00750 } \end{aligned}$ | $\begin{aligned} & \text { N5205 } \\ & \text { W00755 } \end{aligned}$ | 1 | 0 |
| 4166 | 61 | (For this question use annex 061-12581A) <br> Given: <br> SHA VOR (N5243.3 W00853.1) radial $120^{\circ}$, | $\begin{aligned} & \hline \text { N5230 } \\ & \text { W00800 } \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { N5225 } \\ \text { W00805 } \end{array}$ | $\begin{array}{\|l\|} \hline \text { N5220 } \\ \text { W00750 } \end{array}$ | $\begin{aligned} & \text { N5240 } \\ & \text { W00750 } \end{aligned}$ | 1 | 0 |
| 4167 | 61 | (For this question use annex 061-12580A) <br> Given: <br> SHA VOR (N5243.3 W00853.1) radial $205^{\circ}$, | $\begin{array}{\|l\|} \hline \text { N5205 } \\ \text { W009 } 15 \end{array}$ | $\begin{aligned} & \hline \text { N52 15 } \\ & \text { W00917 } \end{aligned}$ | $\begin{aligned} & \text { N5210 } \\ & \text { W00910 } \end{aligned}$ | N51 18 W00913 | 0 | 0 |


| 4168 | 61 | (For this question use annex 061-12579A) <br> Given: <br> SHA VOR (N5243.3 W00853.1) radial $223^{\circ}$, | $\begin{aligned} & \hline \text { N5210 } \\ & \text { W00930 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5220 } \\ & \text { W00920 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5230 } \\ & \text { W00910 } \end{aligned}$ | $\begin{aligned} & \hline \text { N52 10 } \\ & \text { W009 } 10 \end{aligned}$ | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4169 | 61 | (For this question use annex 061-12578A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between CRN NDB (N5318.1 W00856.5) and EKN NDB (N5423.6 | $\begin{array}{lll} 035^{\circ}-80 \\ N M & & \end{array}$ |  $042^{\circ}-83$ <br> $N M$  | $\begin{array}{ll} 036^{\circ}-81 \\ \text { NM } & \end{array}$ | $\begin{array}{lll} 044^{\circ}-82 \\ N M & & \end{array}$ | 1 | 0 | 0 | 0 |
| 4170 | 61 | (For this question use annex 061-12577A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between BAL VOR (N5318.0 W00626.9) and CFN NDB (N5502.6 | $\begin{array}{lll} 327^{\circ}-124 \\ \text { NM } & \end{array}$ | $\begin{array}{lll} 335^{\circ}-128 \\ \text { NM } & \end{array}$ | $\begin{array}{ll} 325^{\circ}-126 \\ N M & \end{array}$ | $\begin{array}{lll} 320^{\circ}-127 \\ N M & \end{array}$ | 1 | 0 | 0 | 0 |
| 4171 | 61 | (For this question use annex 061-12585A) <br> Given: <br> SHA VOR/DME (N5243.3 W00853.1) radial 165\%/36 NM. | $\begin{aligned} & \hline \text { N5210 } \\ & \text { W00830 } \end{aligned}$ | $\begin{aligned} & \text { N5208 } \\ & \text { W00840 } \end{aligned}$ | $\begin{aligned} & \text { N5315 } \\ & \text { W00915 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5317 } \\ & \text { W00908 } \end{aligned}$ | 1 | 0 | 0 | 0 |
| 4172 | 61 | Where and when are the IRS positions updated? | During flight IRS positions are automatically updated by the FMC | IRS positions are updated by pressing the 'Take-off/ Go -around' button at the start of the take-off roll | Updating is normally carried out by the crew when over-flying a known position (VOR station or NDB) | Only on the ground during the alignment procedure | 0 | 0 | 0 | 1 |
| 4173 | 61 | (For this question use annex 061-12560A) <br> What is the radial and DME distance from CON VOR/DME (N5354.8 W00849.1) to position N5330 W00930? | $\begin{aligned} & 165^{\circ}-27 \\ & \text { NM } \end{aligned}$ | $\begin{array}{ll} 335^{\circ}-43 \\ N M & \end{array}$ | $\begin{aligned} & 025^{\circ}-38 \\ & \mathrm{NM} \end{aligned}$ | $\begin{array}{ll} 233^{\circ}-35 \\ N M & \end{array}$ | 0 | 0 | 0 | 1 |
| 4174 | 61 | (For this question refer to annex 061-12602A) <br> Given: <br> CON VOR/DME (N5354.8 W00849.1) <br> Castlebar aerodrome (N5351 W00917) | $\begin{array}{lll} 265^{\circ}-17 \\ \text { NM } & \end{array}$ | $\begin{aligned} & 077^{\circ}-18 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 257^{\circ}-17 \\ & \text { NM } \end{aligned}$ | $\begin{array}{lll} 086^{\circ}-18 \\ \text { NM } & \end{array}$ | 1 | 0 | 0 | 0 |
| 4175 | 61 | (For this question refer to annex 061-12601A) <br> Given: <br> SHA VOR/DME (N5243.3 W00853.1) <br> Connemara aerodrome (N5314 W00928) | $\begin{array}{ll} 154^{\circ}-38 \\ \text { NM } & \end{array}$ | $\begin{aligned} & 326^{\circ}-37 \\ & N M \end{aligned}$ | $\begin{aligned} & 146^{\circ}-38 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 333^{\circ}-37 \\ & N M \end{aligned}$ | 0 | 0 | 0 | 1 |
| 4176 | 61 | An aircraft is descending down a $12 \%$ slope whilst maintaining a GS of 540 kt . <br> The rate of descent of the aircraft is approximately: | $4500 \mathrm{FT} / \mathrm{MIN}$ | 3900 FT/MIN | $6500 \mathrm{FT} / \mathrm{MIN}$ | $650 \mathrm{FT} / \mathrm{MIN}$ | 0 | 0 | 1 | 0 |
| 4177 | 61 | (For this question refer to annex 061-12600A) <br> Given: <br> SHA VOR/DME (N5243.3 W00853.1) <br> Birr aerodrome (N5304 W00754) | $\begin{array}{ll} 240^{\circ}-41 \\ N M & \end{array}$ | $\begin{aligned} & 068^{\circ}-41 \\ & \mathrm{NM} \end{aligned}$ | $\begin{array}{ll} 248^{\circ}-42 \\ N M & \end{array}$ | $\begin{aligned} & 060^{\circ}-42 \\ & \mathrm{Nm} \end{aligned}$ | 0 | 1 | 0 | 0 |
| 4178 | 61 | (For this question use annex 061-12590A) <br> Given: <br> SHA VOR N5243.3 W00853.1 <br> CRK VORN5150.4 W00829.7 | $\begin{aligned} & \text { SHA } 124^{\circ} \\ & \text { CRK } 009^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 131^{\circ} \\ & \text { CRK } 017^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 304^{\circ} \\ & \text { CRK } 189^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 312^{\circ} \\ & \text { CRK } 197^{\circ} \end{aligned}$ | 0 | 1 | 0 | 0 |
| 4179 | 61 | (For this question use annex 061-12598A) <br> Given: <br> CON VOR (N5354.8 W00849.1) DME 30 NM, <br> CRN VOR (N5318.1 W00856.5) DME 25 NM, | $\begin{aligned} & \hline \text { N5330 } \\ & \text { W00820 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5343 } \\ & \text { W00925 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5335 } \\ & \text { W00925 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5337 } \\ & \text { W00820 } \end{aligned}$ | - | - | 0 | - |
| 4180 | 61 | (For this question use annex 061-12574A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between WTD NDB (N521 1.3 W00705.0) and SLG NDB (N5416.7 | $\begin{aligned} & 156^{\circ}-136 \\ & \text { NM } \end{aligned}$ | $\begin{array}{lll} 164^{\circ}-138 \\ N M & & \\ \hline \end{array}$ | $\begin{array}{lll} 336^{\circ}-137 \\ \text { NM } & \end{array}$ | $\begin{array}{lll} 344^{\circ}-139 \\ \text { NM } & \end{array}$ | 0 | 0 | 1 | 0 |


| 4181 | 61 | What is the source of magnetic variation information in a Flight Management System (FMS)? | Magnetic variation is calculated by each IRS based on the respective IRS position and the aircraft magnetic heading | Magnetic variation information is stored in each IRS memory; it is applied to the true heading calculated by the respective IR S | The main directional gyro which is coupled to the magnetic sensor (flux valve) positioned in the wingtip | The FMS calculates MH and MT from the FMC position | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4182 | 61 | (For this question use annex 061-12597A) <br> Given: <br> CRN VOR (N5318.1 W00856.5) DME 34 NM, <br> SHA VOR (N5243.3 W00853.1) DME 26 NM, | $\begin{aligned} & \text { N5255 } \\ & \text { W00815 } \end{aligned}$ | N5250 W0030 | $\begin{aligned} & \text { N5305 } \\ & \text { W00930 } \end{aligned}$ | $\begin{aligned} & \text { N5310 } \\ & \text { W00820 } \end{aligned}$ | 1 | 0 |  | 0 |
| 4183 | 61 | (For this question use annex 061-12596A) <br> Given: <br> CRN VOR (N5318.1 W00856.5) DME 18 NM, <br> SHA VOR (N5243.3 W00853.1) DME 30 NM, | $\begin{aligned} & \text { N5307 } \\ & \text { W00923 } \end{aligned}$ | $\begin{aligned} & \text { N5355 } \\ & \text { W00825 } \end{aligned}$ | $\begin{aligned} & \text { N5310 } \\ & \text { W00830 } \end{aligned}$ | $\begin{aligned} & \hline \text { N5252 } \\ & \text { W00923 } \end{aligned}$ | 0 | 0 | 1-1 | 0 |
| 4184 | 61 | (For this question use annex 061-12595A) <br> Given: <br> SHA VOR (N5243.3 W00853.1) DME 41 NM, <br> CRK VOR (N5150.4 W00829.7) DME 30 NM, | $\begin{aligned} & \text { N5225 } \\ & \text { W00810 } \end{aligned}$ | N5215 W00805 | $\begin{aligned} & \text { N5205 } \\ & \text { W00915 } \end{aligned}$ | $\begin{aligned} & \text { N5215 } \\ & \text { W00915 } \end{aligned}$ | 0 | 1-1 |  | 0 |
| 4185 | 61 | (For this question use annex 061-12594A) <br> Given: <br> SHA VOR (N5243.3 W00853.1) DME 50 NM, <br> CRK VOR (N5150.4 W00829.7) DME 41 NM, | $\begin{aligned} & \text { N5235 } \\ & \text { W00750 } \end{aligned}$ | $\begin{aligned} & \text { N5200 } \\ & \text { W00935 } \end{aligned}$ | $\begin{aligned} & \text { N5215 } \\ & \text { W00940 } \end{aligned}$ | $\begin{aligned} & \text { N5215 } \\ & \text { W00745 } \end{aligned}$ | 0 | 1-1 | - | 0 |
| 4186 | 61 | (For this question use annex 061-12593A) <br> Given: <br> SHA VOR N5243.3 W00853.1 <br> CON VOR N5354.8 W00849.1 | $\begin{aligned} & \text { SHA } 137^{\circ} \\ & \text { CON 046 } \end{aligned}$ | $\begin{aligned} & \text { SHA } 317^{\circ} \\ & \text { CON } 226^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 145^{\circ} \\ & \text { CON } 055^{\circ} \end{aligned}$ | $\begin{aligned} & \text { SHA } 325^{\circ} \\ & \text { CON } 235^{\circ} \end{aligned}$ | - | - | - | 1 |
| 4187 | 61 | (For this question refer to annex 061-12599A) <br> Given: <br> CRK VOR/DME (N5150.4 W00829.7) <br> Kerrv aerodrome (N5210.9 W00931.4) | $\begin{array}{lll} 119^{\circ}-44 \\ \text { NM } & & \end{array}$ | $\begin{aligned} & 127^{\circ}-45 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 299^{\circ}-42 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 307^{\circ}-43 \\ & N M \end{aligned}$ | - | 0 | - | 1 |
| 4188 | 61 | Which of the following lists, which compares an Inertial Reference System that utilises Ring Laser Gyroscopes (RLG) instead of conventional gyroscopes, is completely correct? | The platform is kept stable relativ e to the earth mathematicall y rather than mechanically but it has a longer 'spin up' time | It does not suffer from 'lock in' error and it is insensitive to gravitation al ('g') forces | There is little or no 'spin up' time and it does not suffer from 'lock in' error | There is little or no 'spin up' time and it is insensitive to gravitation al ('g') forces | 0 | 0 | 0 | 1 |
| 4189 | 61 | Gyrocompassing of an inertial reference system (IRS) is accomplished with the mode selector switched to: | ON | ALIGN | STBY | ATT/REF | 0 | 1 | 0 | 0 |
| 4190 | 61 | With reference to an inertial navigation system (INS), the initial great circle track between computer inserted waypoints will be displayed when the control display unit (CDU) is selected to: | HDG/DA | TK/GS | XTK/TKE | DSRTK/STS | 0 | 0 | 0 | 1 |


| 419 | 61 | Which of the following statement is correct concerning gyro-compassing of an inertial navigation system (INS)? | Gyro-compas sing of an INS is not possible in flight because it cannot differentiate between movement induced and misalignment induced accelerations | Gyro-compas sing of an INS is possible in flight because it can differentiate between movement induced and misalignment induced accelerations | Gyro-compas sing of an INS is possible in flight because it cannot differentiate between movement induced and misalignment induced accelerations | Gyro-compas sing of an INS is not possible in flight because it can differentiate between movement induced and misalignment induced accelerations | 1 | 0 | 00 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4192 | 61 | During the initial alignment of an inertial navigation system (INS) the equipment: | will accept a $10^{\circ}$ error in initial latitude and initial longitude | will not accept a $10^{\circ}$ error in initial latitude but will accept a $10^{\circ}$ error in initial longitude | will accept a $10^{\circ}$ error in initial latitude but will not accept a $10^{\circ}$ error in initial longitude | will not accept a $10^{\circ}$ error in initial latitude or initial longitude | 0 | 1 | 00 |  |
| 4193 | 61 | Double integration of the output from the east/west accelerometer of an inertial navigation system (INS) in the NAV MODE give: | velocity east/west | distance east/west | vehicle longitude | distance north/south | 0 | 1 | 00 | 0 |
| 4194 | 61 | (For this question use annex 061-12576A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between BAL VOR (N5318.0 W00626.9) and CRN NDB (N5318.1 | $\begin{array}{lll} 268^{\circ}-91 \\ N M & & \end{array}$ | $\begin{aligned} & 272^{\circ}-89 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 270^{\circ}-90 \\ & \text { NM } \end{aligned}$ | $\begin{array}{ll} 278^{\circ}-89 \\ N M & \end{array}$ | 0 | 0 | 10 | 0 |
| 4195 | 61 | The principle of 'Schuler Tuning' as applied to the operation of Inertial Navigation Systems/ Inertial Reference Systems is applicable to: | both gyro-stabilise d platform and 'strapdown' systems | only gyro-stabilise d systems | both gyro-stabilise d and laser gyro systems but only when operating in the non 'strapdown' mode | only to 'strapdown' laser gyro systems | 1 | 0 |  |  |
| 4196 | 61 | The automatic flight control system is coupled to the guidance outputs from an inertial navigation system. <br> Which pair of latitudes will give the greatest difference between initial track read-out and the average true course given, in each case, a difference of longitude of $10^{\circ}$ ? | $\begin{aligned} & 60^{\circ} \mathrm{N} \text { to } \\ & 60^{\circ} \mathrm{N} \end{aligned}$ | $\begin{aligned} & 60^{\circ} \mathrm{N} \text { to } \\ & 50^{\circ} \mathrm{N} \end{aligned}$ | $\begin{aligned} & 30^{\circ} \mathrm{S} \text { to } \\ & 30^{\circ} \mathrm{N} \end{aligned}$ | $30^{\circ} \mathrm{S}$ to $25^{\circ} \mathrm{S}$ | 1 | 0 | 00 | 0 |
| 4197 | 61 | The resultant of the first integ ration of the output from the east/west accelerometer of an inertial navigation system (INS) in NAV MODE is: | change of longitude | vehicle longitude | departure | velocity along the local parallel of latitude | 0 | - | 0 | 1 |
| 4198 | 61 | One of the errors inherent in a ring laser gyroscope occurs at low input rotation rates tending towards zero when a phenomenon known as 'lock-in' is experienced. What is the name of the technique, effected by means of a piezo-electric motor, that is used to correct this error? | cavity rotation | zero drop | beam lock | dither | 0 | 0 | 01 | 1 |
| 4199 | 61 | (For this question use annex 061-9442A) <br> Complete line 6 of the 'FLIGHT NAVIGATION LOG', positions 'L' to 'M'. | HDG $064^{\circ}$ <br> ETA 1449 <br> UTC | $\begin{aligned} & \text { HDG } 075^{\circ}- \\ & \text { ETA } 1452 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 070^{\circ}- \\ & \text { ETA } 1459 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 075^{\circ}- \\ & \text { ETA } 1502 \\ & \text { UTC } \end{aligned}$ | 0 | 0 | 01 | - |
| 4200 | 61 | (For this question use annex 061-9441A) <br> Complete line 5 of the 'FLIGHT NAVIGATIONLOG', positions 'J' to 'K'. | $\begin{aligned} & \text { HDG } 337^{\circ}- \\ & \text { ETA } 1422 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 320^{\circ}- \\ & \text { ETA } 1412 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 337^{\circ}- \\ & \text { ETA } 1322 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 320^{\circ}- \\ & \text { ETA } 1432 \\ & \text { UTC } \end{aligned}$ | 1 | 0 | 0-1 | 0 |


| 4201 | 61 | (For this question use annex 061-9440A) <br> Complete line 4 of the 'FLIGHT NAVIGATION LOG', positions 'G' to 'H'. | $\begin{aligned} & \text { HDG } 344^{\circ}- \\ & \text { ETA } 1303 \\ & \text { UTC } \end{aligned}$ | HDG $344^{\circ}-$ ETA 1336 UTC | $\begin{aligned} & \text { HDG } 354^{\circ}- \\ & \text { ETA } 1326 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 034^{\circ} \text { - } \\ & \text { ETA } 1336 \\ & \text { UTC } \end{aligned}$ | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4202 | 61 | (For this question use annex 061-9439A) <br> Complete line 3 of the 'FLIGHT NAVIGATIONLOG', positions 'E' to 'F'. | $\begin{aligned} & \text { HDG } 095^{\circ}- \\ & \text { ETA } 1155 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 106^{\circ}- \\ & \text { ETA } 1215 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 115^{\circ}- \\ & \text { ETA } 1145 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 105^{\circ}- \\ & \text { ETA } 1205 \\ & \text { UTC } \end{aligned}$ | 0 | 0 | 0 | 1 |
| 4203 | 61 | The resultant of the first integration from the north/south accelerometer of an inertial navigation system (INS) in the NAV MODE is: | change latitude | latitude | velocity along the local meridian | groundspeed | 0 | 0 | 1 | 0 |
| 4204 | 61 | Given: ILS GP angle = 3.5 DEG , | 900 FT/MIN | $1000 \mathrm{FT} / \mathrm{MIN}$ | $700 \mathrm{FT} / \mathrm{MIN}$ | 800 FT/MIN | 1 | 0 | 0 | 0 |
| 4205 | 61 | (For this question refer to annex 061-12605A) <br> What feature is shown on the chart at position N5212 | Clonbullogue aerodrome | TUSKAR ROCKLT.H. NDB | WTD NDB | KERRY/Farra nfore aerodrome | 0 | 1 | 0 | 0 |
| 4206 | 61 | (For this question use annex 061-12573A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between WTD NDB (N521 1.3 W00705.0) and FOY NDB (N5234.0 | $\begin{aligned} & 286^{\circ}-81 \\ & N M \end{aligned}$ | $\begin{aligned} & 294^{\circ}-80 \\ & \text { NM } \end{aligned}$ | $\begin{array}{ll} 075^{\circ}-81 \\ \text { NM } & \end{array}$ | $\begin{aligned} & 277^{\circ}-83 \\ & \text { NM } \end{aligned}$ | 1 | 0 | 0 | 0 |
| 4207 | 61 | (For this question use annex 061-12572A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between SLG NDB (N5416.7 W00836.0) and CFN NDB (N5502.6 | $\begin{array}{ll} 011^{\circ}-47 \\ \text { NM } & \end{array}$ | $\begin{array}{ll} \hline 020^{\circ}-46 \\ N M & \end{array}$ | $\begin{array}{ll} 348^{\circ}-46 \\ N M & \end{array}$ | $\begin{aligned} & 191^{\circ}-45 \\ & \text { NM } \end{aligned}$ | 1 | 0 | 0 | 0 |
| 4208 | 61 | (For this question use annex 061-12571A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between CON VOR (N5354.8 W00849.1) and BEL VOR (N5439.7 | $\begin{array}{ll} 113^{\circ}-97 \\ \text { NM } & \\ \hline \end{array}$ | $\begin{aligned} & 293^{\circ}-98 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 063^{\circ}-101 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 071^{\circ}-100 \\ & N M \end{aligned}$ | 0 | - | 1 | 0 |
| 4209 | 61 | (For this question use annex 061-12570A) <br> What is the average track ( ${ }^{\circ} \mathrm{M}$ ) and distance between CRN NDB (N531 8.1 W00856.5) and BEL VOR (N5439.7 | $\begin{aligned} & 089^{\circ}-95 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 229^{\circ}-125 \\ & \text { NM } \end{aligned}$ | $\begin{array}{lll} 237^{\circ}-130 \\ \text { NM } & & \\ \hline \end{array}$ | $\begin{aligned} & 057^{\circ}-126 \\ & \text { NM } \end{aligned}$ | 0 | 0 | 0 | 1 |
| 4210 | 61 | (For this question use annex 061-12569A) <br> What is the average track ( ${ }^{\circ} \mathrm{M}$ ) and distance between BAL VOR (N5318.0 W00626.9) and SLG NDB (N54 16.7 | $\begin{array}{ll} \hline 262^{\circ}-86 \\ N M & \end{array}$ | $\begin{aligned} & 128^{\circ}-99 \\ & \text { NM } \end{aligned}$ | $\begin{array}{ll} 308^{\circ}-98 \\ N M & \end{array}$ | $\begin{aligned} & 316^{\circ}-96 \\ & \text { NM } \end{aligned}$ | 0 | 0 | 0 | 1 |
| 4211 | 61 | The following points are entered into an inertial navigation system (INS). <br> WPT 1: $\quad 60^{\circ} \mathrm{N} 30^{\circ} \mathrm{W}$ <br> WPT 2: $\quad 60^{\circ} \mathrm{N} 20^{\circ} \mathrm{W}$ <br> WPT 3: $\quad 60^{\circ} \mathrm{N} \quad 10^{\circ} \mathrm{W}$ <br> The inertial navigation system is connected to the automatic | zero | a $9^{\circ}$ increase | a $4^{\circ}$ decrease | a $9^{\circ}$ decrease | 0 |  |  | 1 |
| 4212 | 61 | Given: <br> aircraft height 2500 FT, ILS GP angle $3^{\circ}$. | 8.3 NM | 7.0 NM | 13.1 NM | 14.5 NM | 1 | 0 | 0 | 0 |
| 4213 | 61 | The automatic flight control system (AFCS) in an aircraft is coupled to the guidance outputs from an inertial navigation system (INS) and the aircraft is flying from waypoint No. 2 $\left(60^{\circ} 00^{\prime} \mathrm{S} 070^{\circ} 00^{\prime} \mathrm{W}\right)$ to No. 3 ( $60^{\circ} 00^{\prime} \mathrm{S} 080^{\circ} 00^{\prime} \mathrm{W}$ ). <br> Comparing the initial track $\left({ }^{\circ} \mathrm{T}\right)$ at $070^{\circ} 00^{\prime} \mathrm{W}$ and the final track ( ${ }^{\circ} \mathrm{T}$ ) at $080^{\circ} 00^{\prime} \mathrm{W}$, the difference between them is that the initial track is approximately: | $9^{\circ}$ greater than the final one | $5^{\circ}$ less than the final one | $9^{\circ}$ less than the final one | $5^{\circ}$ greater than the final one | 0 | 0 | 1 | 0 |
| 4214 | 61 | Given: $\text { TAS = } 197 \mathrm{kt},$ <br> True course $=240^{\circ}$, $\mathrm{W} / \mathrm{V}=180 / 30 \mathrm{kt} .$ <br> Descent is initiated at FL 220 and completed at FL 40. | $800 \mathrm{FT} / \mathrm{MIN}$ | 950 FT/MIN | $1500 \mathrm{FT} / \mathrm{MIN}$ | 1400 FT/MIN | 0 | 0 | 0 | 1 |


| 4215 | 61 | What is the effect on the Mach number and TAS in an aircraft that is climbing with constant CAS? | Mach number rema ins constant; TAS increases | Mach number decr eases; TAS decreases | Mach number incre ases; TAS remains constant | Mach number incre ases; TAS increases | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4216 | 61 | Which of the following statements conceming the earth's magnetic field is completely correct? | Dip is the angle between total magneti c field and vertical field component | The blue pole of the earth's magnetic field is situated in North Canada | At the earth's magnetic equator, the inclination varies depending on whether the geograhic equator is north or south of the magnetic equator | The earth's magnetic field can be classified as transient, semi-perman ent or permanent | 0 | 1 |
| 4217 | 61 | Which of the following correctly lists the order of available selections of the Mode Selector switches of an inertial reference system (IRS) mode panel? | $\begin{aligned} & \text { OFF - } \\ & \text { ALIGN - } \\ & \text { NAV - ATT } \end{aligned}$ | $\begin{aligned} & \text { OFF - ON - } \\ & \text { ALIGN - } \\ & \text { NAV } \end{aligned}$ | $\begin{aligned} & \hline \text { OFF - } \\ & \text { STBY - } \\ & \text { ALIGN } \\ & \text { NAV } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { OFF - } \\ & \text { ALIGN - } \\ & \text { ATT - NAV } \end{aligned}$ | 1 | 0 |
| 4218 | 61 | The automatic flight control system (AFCS) in an aircraft is coupled to the guidance outputs from an inertial navigation system (INS). <br> The aircraft is flying between inserted waypoints No. 3 ( $55^{\circ} 00^{\prime} \mathrm{N} 020^{\circ} 00^{\prime} \mathrm{W}$ ) and No. 4 ( $55^{\circ} 00^{\prime} \mathrm{N} 030^{\circ} 00^{\prime} \mathrm{W}$ ). <br> With DSRTK/STS selected on the CDU, to the nearest whole degree, the initial track read-out from waypoint No. 3 will be: | $266^{\circ}$ | $270^{\circ}$ | $274^{\circ}$ | $278^{\circ}$ | 0 |  |
| 4219 | 61 | (For this question use annex 061-12575A) <br> What is the average track ( ${ }^{\circ} \mathrm{T}$ ) and distance between SHA VOR (N5243.3 W00853.1) and CON VOR (N5354.8 | $\begin{array}{ll} 010^{\circ}-71 \\ \text { NM } & \end{array}$ | $\begin{aligned} & 358^{\circ}-72 \\ & N M \end{aligned}$ | $\begin{aligned} & 006^{\circ}-71 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 002^{\circ}-72 \\ & N M \end{aligned}$ | 0 | 0 |
| 4220 | 61 | (For this question use annex 061-12568A) <br> What is the average track ( ${ }^{\circ} \mathrm{M}$ ) and distance between KER NDB (N5210.9 W00931.5) and CRN NDB (N5318.1 | $\begin{array}{ll} 205^{\circ}-71 \\ N M & \end{array}$ | $\begin{array}{ll} 017^{\circ}-70 \\ \text { NM } & \end{array}$ | $\begin{aligned} & 025^{\circ}-70 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 197^{\circ}-71 \\ & N M \end{aligned}$ | 0 | 0 |
| 4221 | 61 | The direct reading magnetic compass is made aperiodic (dead beat) by: | using long magnets | pendulous suspension of the magnetic assembly | keeping the magnetic assembly mass close to the compass point and by using damping wires | using the lowest acceptable viscosity compass liquid | 0 | 0 |
| 4222 | 61 | (For this question refer to annex 061-12603A) <br> Given: <br> CON VOR/DME (N5354.8 W00849.1) <br> Abbey Shrule aerodrome (N5335 W00739) | $\begin{aligned} & 296^{\circ}-46 \\ & N M \end{aligned}$ | $\begin{aligned} & 304^{\circ}-47 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 124^{\circ}-46 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 116^{\circ}-47 \\ & N M \end{aligned}$ | 0 | 0 |
| 4223 | 61 | What is the validity period of the 'permanent' dat a base of aeronautical information stored in the FMC In the B737-400 Flight Management System? | 28 days | one calendar month | 3 calendar months | 14 days | 1 | 0 |
| 4224 | 61 | What indication, if any, is given in the B737-400 Flight Management System if radio updating is not available? | A waming message is displayed on the Flight Director System | No indication is given so long as the IRS positions rem ain within limits | A waming message is displayed on the EHSI and MFDU | A waming message is displayed on the IRS displays | 0 | 0 |


| 4225 | 61 | Which component of the B737-400 Flight Management System (FMS) is used to enter flight plan routeing and performance parameters? | Multi-Function Control Display Unit | Flight <br> Management Computer | Inertial <br> Reference System | Flight Director Syst em | 1 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4226 | 61 | The purpose of the Flight Management System (FMS), as for example installed in the B737-400, is to provide: | both manual navigation guidance and performa nce management | continuous automatic navigation guidance and performa nce management | manual navigation guidance and automati c performance management | continuous automatic navigation guidance as well as manual performance management | 0 | 1 | 0 | 0 |
| 4227 | 61 | How is the radio position determined by the FMC in the B737-400 Electronic Flight Instrument System? | DME/DME | DME/DME or VOR/DME | DME ranges and/ or VOR/ADF bearings | VOR/DME range and bearing | 1 | 0 | 0 | 0 |
| 4228 | 61 | A direct reading compass should be swung when: | the aircraft has made more than a stated number of landings | there is a large, and permanent, change in magnetic latitude | there is a large change in magnetic longitude | the aircraft is stored for a long period and is frequently moved | 0 | 1 | 0 | 0 |
| 4229 | 61 | In which of the following situations is the FMC present position of a B737-400 Electronic Flight Instrument System likely to be least accurate? | Just after take-off | At top of climb | At top of descent | On final approach | 1 | 0 | 0 | 0 |
| 4230 | 61 | The annunciator of a remote indicating compass system is used when: | synchronising the magnetic and gyro compass elements | compensating for deviation | setting local magnetic variation | setting the 'heading' pointer | 1 | 0 | 0 | 0 |
| 4231 | 61 | The convergence factor of a Lambert conformal conic chart is quoted as 0.78535 . <br> At what latitude on the chart is earth convergency correctly | 38¹5' | $51^{\circ} 45{ }^{\prime}$ | $52^{\circ} 05^{\prime}$ | 80³9' | 0 | 1 | 0 | 0 |
| 4232 | 61 | At $47^{\circ}$ North the chart distance between meridians $10^{\circ}$ apart is 5 inches. | 1:8000 000 | 1:3000 000 | 1:2500 000 | 1:6000 000 | 0 | 0 | 0 | 1 |
| 4233 | 61 | On a Direct Mercator chart a great circle will be represented by a: | curve convex to the equator | straight line | curve concave to the equator | complex curve | 0 | 0 | 1 | 0 |
| 4234 | 61 | An aircraft in the northern hemisphere is making an accurate rate one turn to the right. <br> If the initial heading was $135^{\circ}$, after 30 seconds the direct reading magnetic compass should read: | $225^{\circ}$ | $\begin{aligned} & \text { less than } \\ & 225^{\circ} \end{aligned}$ | more or less than $225^{\circ}$ depending on the pendulous suspension used | more than $225^{\circ}$ | 0 | 0 | 0 | 1 |
| 4235 | 61 | When accelerating on a westerly heading in the northern hemisphere, the compass card of a direct reading magnetic compass will turn: | clockwise giving an apparent tum towards the north | clockwise giving an apparent tum towards the south | anti-clockwise giving an apparent tum towards the north | anti-clockwise giving an apparent tum towards the south |  | 0 | - | 0 |
| 4236 | 61 | On a Lambert conformal conic chart, with two standard parallels, the quoted scale is correct: | along the prime meridian | along the two standard parallels | in the area between the standard parallels | along the parallel of origin | 0 | 1 | 0 | - |
| 4237 | 61 | (For this question refer to annex 061-12615A) <br> Which of the aeronautical chart symbols indicates a DME? | 6 | 2 | 3 | 5 | 0 | 1 | 0 | 0 |
| 4238 | 61 | (For this question refer to annex 061-12623A) <br> Which aeronautical chart symbol indicates a Control Zone | 2 | 3 | 4 | 5 | 0 | 1 | 0 | 0 |
| 4239 | 61 | (For this question refer to annex 061-12621A) <br> Which aeronautical chart symbol indicates a Flight | 1 | 3 | 4 | 5 | 1 | 0 | 0 | 0 |


| 4240 | 61 | (For this question refer to annex 061-1 2620A) <br> Which of the aeronautical chart symbols indicates a | 3 | 6 | 7 | 1 | 0 | 0 | 10 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4241 | 61 | (For this question refer to annex 061-12619A) <br> Which of the aeronautical chart symbols indicates a TACAN? | 6 | 7 | 1 | 2 | 1 | 0 | 0 | 0 |
| 4242 | 61 | (For this question refer to annex 061-12618A) <br> Which of the aeronautical chart symbols indicates a basic, | 5 | 6 | 2 | 3 | 1 | 0 | 0 | 0 |
| 4243 | 61 | In the B737-400 Flight Management System the CDUs are used during preflight to: | manually initialize the IRSs, FMC and Autothrottle with dispatch information | manually initialize the IRSs and FMC with dispatch information | automatically initialize the IRSs and FMC with dispatch information | manually initialize the Flight Director Syst em and FMC with dispatch information | 0 |  | 1 |  |
| 4244 | 61 | (For this question refer to annex 061-12616A) <br> Which of the aeronautical chart symbols indicates a VOR? | 3 | 5 | 6 | 2 | 1 | 0 | 0 | 0 |
| 4245 | 61 | (For this question refer to annex 061-12613A) <br> Which of the following lists all the aeronautical chart symbols | VOR: NDB | civil aiport: ILS | NDB: ILS | civil airport: NDB | 0 | 0 | 0 | 1 |
| 4246 | 61 | (For this question refer to annex 061-12614A) <br> Which of the aeronautical chart symbols indicates a | 6 | 7 | 1 | 2 | 0 | 0 | 1 | 0 |
| 4247 | 61 | Which of the following lists the first three pages of the FMC/CDU normally used to enter data on initial start-up of the B737-400 Electronic Flight Instrument System? | POS INIT RTE - IDENT | $\begin{array}{\|l\|} \hline \text { IDENT - RTE } \\ \hline \text { DEPARTURE } \end{array}$ | POS INIT <br> RTE - <br> DEPARTUR <br> E | IDENT - POS <br> INIT - RTE | 0 | 0 | 0 | 1 |
| 4248 | 61 | Which FMC/CDU page nomally appears on initial power application to the B737-400 Electronic Fight Instrument System? | INITIAL | POS INIT | PERF INIT | IDENT | 0 | 0 | 0 | 1 |
| 4249 | 61 | Which of the following lists all the methods that can be used to enter 'Created Waypoints' into the CDU of a B737-400 Electronic Flight Instrument System? | Identifier bearing/dista nce; place distance/plac e distance; along-track displacement ; latitude and longitude | Identifier bearing/dista nce; place bearing/place bearing; along-track displacement ; latitude and longitude | Identifier bearing/dista nce; place bearing/place distance; along/acrosstrack displacement ; latitude and Iongitude | Identifier bearing/dista nce; place bearing/place bearing; latitude and longitude; waypoint name | 0 | 1 | 0 |  |
| 4250 | 61 | Which of the following can all be stored as five letter waypoint identifiers through the CDU of a B737-400 Electronic Flight Instrument System? | Waypoint names; navaid frequencies; runway codes; airport ICAO identifiers | Waypoint names; navaid positions; airport ICAO identifiers; airport names | Waypoint names; navaid identifiers; runway numbers; airport ICAO identifiers | Airway names; navaid identifiers; airport names; waypoint code numbers | 0 | 0 | 1 |  |
| 4251 | 61 | What are, in order of highest priority followed by lowest, the two levels of message produced by the CDU of the B737-400 Electronic Flight Instrument System? | Urgent and Routine | Priority and Alerting | Urgent and Advisory | Alerting and Advisory | 0 | 0 | 0 | 1 |
| 4252 | 61 | (For this question refer to annex 061-12617A) <br> Which of the aeronautical chart symbols indicates an NDB? | 2 | 3 | 4 | 6 | 0 | 0 | 1 | 0 |
| 4253 | 61 | ATT Mode of the Inertial Reference System (IRS) is a back-up mode providing: | only attitude information | navigation information | altitude, heading and position information | only attitude and heading information |  | 0 |  |  |


| 4254 | 61 | Permanent magnetism in aircraft arises chiefly from: | the combined effect of aircraft electrical equipment and the earth's magnetic field | the effect of intemal wiring and exposure to electrical stoms | hammering, and the effect of the earth's magnetic field, whilst under construction | exposure to the earth's magnetic field during normal operation | 0 | 0 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4255 | 61 | An island appears $30^{\circ}$ to the left of the centre line on an airbome weather radar display. What is the true bearing of the aircraft from the island if at the time of observation the aircraft was on a magnetic heading $(\mathrm{MH})$ of $020^{\circ}$ with the magnetic variation (VAR) $25^{\circ} \mathrm{W}$ ? | $325^{\circ}$ | $145^{\circ}$ | 195 ${ }^{\circ}$ | $205^{\circ}$ | 0 | 1 | 00 |
| 4256 | 61 | An island appears $30^{\circ}$ to the right of the centre line on an airbome weather radar display. What is the true bearing of the aircraft from the island if at the time of observation the aircraft was on a magnetic heading $(\mathrm{MH})$ of $355^{\circ}$ with the magnetic variation (VAR) $15^{\circ} \mathrm{E}$ ? | $130^{\circ}$ | $160^{\circ}$ | $190^{\circ}$ | $220^{\circ}$ | 0 | 0 | 01 |
| 4257 | 61 | An island appears $45^{\circ}$ to the right of the centre line on an airbome weather radar display. What is the true bearing of the aircraft from the island if at the time of observation the aircraft was on a magnetic heading $(\mathrm{MH})$ of $215^{\circ}$ with the magnetic variation (VAR) $21^{\circ} \mathrm{W}$ ? | $329^{\circ}$ | $059^{\circ}$ | $101^{\circ}$ | $239^{\circ}$ | 0 | 1-10 | 00 |
| 4258 | 61 | An island appears $60^{\circ}$ to the left of the centre line on an airbome weather radar display. What is the true bearing of the aircraft from the island if at the time of observation the aircraft was on a magnetic heading $(\mathrm{MH})$ of $276^{\circ}$ with the magnetic variation (VAR) $10^{\circ} \mathrm{E}$ ? | 086 ${ }^{\circ}$ | $226^{\circ}$ | 026 ${ }^{\circ}$ | 046 ${ }^{\circ}$ | 0 | 0 | 01 |
| 4259 | 61 | Waypoints can be entered in an INS memory in different formats. <br> In which of the following formats can waypoints be entered | bearing and distance | hexadecimal | by waypoints name | geographic coordinates | 0 | 0 | 01 |
| 4260 | 61 | Which of the following statements conceming the position indicated on the Inertial Reference System (IRS) display is correct? | The positions from the two IRSs are compared to obtain a'best position' which is displayed on the IRS | It is not updated once the IRS mode is set to NAV | It is constantly updated from informat ion obtained by the FMC | It is updated when 'go-around' is selected on take-off | - | 1 | 0 |
| 4261 | 61 | What additional information is required to be input to an Inertial Navigation System (INS) in order to obtain an W/V readout? | Mach Number | TAS | IAS | Altitude and OAT | 0 | 1 | 00 |
| 4262 | 61 | An aircraft departs from position $\mathrm{A}\left(04^{\circ} 10^{\prime} \mathrm{S} 178^{\circ} 22^{\prime} \mathrm{W}\right)$ and flies northward following the meridian for 2950 NM . It then flies westward along the parallel of latitude for 382 NM to position B. | $\begin{aligned} & 53^{\circ} 20^{\prime} \mathrm{N} \\ & 172^{\circ} 38^{\prime} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 45^{\circ} 00^{\prime} \mathrm{N} \\ & 172^{\circ} 38^{\prime} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 53^{\circ} 20^{\prime} \mathrm{N} \\ & 169^{\circ} 22 \mathrm{~W} \end{aligned}$ | $\begin{aligned} & 45^{\circ} 00^{\prime} \mathrm{N} \\ & 169^{\circ} 22 \mathrm{~W} \end{aligned}$ | 0 | 1 | 00 |
| 4263 | 61 | The angle between the true great-circle track and the true rhumb-line track joining the following points: A $60^{\circ} \mathrm{S} 165^{\circ}$ W) $B\left(60^{\circ} S 177^{\circ} \mathrm{E}\right)$, at the place of departure A , is: | $7.8^{\circ}$ | $9^{\circ}$ | $15.6^{\circ}$ | $5.2^{\circ}$ | 1 | 0 | 00 |
| 4264 | 61 | Given: Waypoint $1.60^{\circ} \mathrm{S} 030^{\circ} \mathrm{W}$ <br> Waypoint 2. $60^{\circ} \mathrm{S} 020^{\circ} \mathrm{W}$ <br> What will be the approximate latitude shown on the display | 06011'S | 05949'S | 06000'S | 06006'S | 0 | 0 | 01 |
| 4265 | 61 | What is the time required to travel along the parallel of latitude $60^{\circ} \mathrm{N}$ between meridians $010^{\circ} \mathrm{E}$ and $030^{\circ} \mathrm{W}$ at a groundspeed of 480 kt ? | 5 HR 00 MIN | 2 HR 30 MIN | 1 HR 15 MIN | 1 HR 45 MIN | 0 | 1 | 0 |
| 4266 | 61 | (For this question refer to annex 061-12607A) <br> What feature is shown on the chart at position N5351 | Brittas Bay aerodrome | Castlebar aerodrome | Connaught aerodrome | Connemara aerodrome | 0 |  | 0 |


| 4267 | 61 | (For this question refer to annex 061-12606A) <br> What feature is shown on the chart at position N5311 | Punchestown aerodrome | Connemara aerodrome | KERRY/Farra nfore aerodrome | Clonbullogue aerodrome | 1 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4268 | 61 | Which of the following statements conceming the loss of alignment by an Inertial Reference System (IRS) in flight is correct? | It is not usable in any mode and must be shut down for the rest of the flight | The navigation mode, including present position and ground speed output s , is inoperative for the remainder of the flight | The IRS has to be coupled to the remaining serviceable system and a realignmen t carried out in flight | The mode selector has to be rotated to ATT then back through ALIG N to NAV in order to obtain an in-flight realignment | 0 | 1 | 0 | 0 |
| 4269 | 61 | The two standard parallels of a conical Lambert projection are at $\mathrm{N} 10^{\circ} 40^{\prime} \mathrm{N}$ and $\mathrm{N} 41^{\circ} 20^{\prime}$. <br> The cone constant of this chart is approximatively : | 0.90 | 0.66 | 0.18 | 0.44 | 0 | 0 | 0 | 1 |
| 4270 | 61 | Given: <br> Distance ' A ' to ' B ' is 90 NM, <br> Fix obtained 60 NM along and 4 NM to the right of course. <br> What heading alteration must be made to reach 'B'? | $4^{\circ}$ Left | $8^{\circ}$ Left | $12^{\circ}$ Left | $16^{\circ}$ Left | 0 | 0 | 1 | 0 |
| 4271 | 61 | (For this question refer to annex 061-12612A) <br> Which of the following lists all the aeronautical chart symbols shown at position N5318.1 W00856.5? | VOR: DME: NDB: compulsory reporting point | civil airport: VOR: DME: non-compulso ry reporting point | VOR: DME: NDB: compulsory reporting point | civil aiport: NDB: DME: non-compuls ory reporting point | 0 | 0 | 0 | 1 |
| 4272 | 61 | (For this question refer to annex 061-12611A) <br> Which of the following lists all the aeronautical chart symbols shown at position N5416.7 W00836.0? | civil aiport: NDB: DME: compulsory reporting point | VOR: DME: NDB: compulsory reporting point | civil aimport: VOR: DME: non-compulso ry reporting point | VOR: DME: NDB: non-compuls ory reporting point | 1 | 0 | 0 | 0 |
| 4273 | 61 | (For this question refer to annex 061-12610A) <br> Which of the following lists all the aeronautical chart symbols shown at position N5318.0 W00626.9? | military airport: VOR: NDB | VOR: DME: danger area | military airport: VOR: DME | civil airport: VOR: DME | 0 | 0 | 1 | 0 |
| 4274 | 61 | (For this question refer to annex 061-12609A) <br> Which of the following lists all the aeronautical chart symbols shown at position N5150.4 W00829.7? | VOR: DME: <br> NDB:compul sory reporting poi nt | VOR: DME: NDB: ILS | civil aiport: VOR: DME: compulsory reporting point | civil aiport: VOR: non-compuls ory reporting point | 0 | 0 | 1 | 0 |
| 4275 | 61 | (For this question refer to annex 061-12608A) <br> What feature is shown on the chart at position N5417 | Belmullet aerodrome | Carnmore aerodrome | Clonbullogue aerodrome | $\begin{array}{\|l} \hline \text { EAGLE } \\ \text { ISLAND } \\ \text { LT.H. NDB } \end{array}$ | 0 | 0 | 0 | 1 |
| 4276 | 61 | The main reason for usually mounting the detector unit of a remote indicating compass in the wingtip of an aeroplane is to: | place it where it will not be subjected to electrical or magnetic interference from the aircraft | reduce the amount of deviation caused by aircraft magnetism and electrical circ uits | facilitate easy mainten ance of the unit and increase its exposure to the Earth's magnetic field | place it in a position where there is no electrical wiring to cause deviation errors | 0 | 1-1 | 0 | 0 |
| 4277 | 61 | Given: <br> Position ' A ' is $\mathrm{N} 00^{\circ} \mathrm{E} 100^{\circ}$, | $\begin{aligned} & \text { N01̊} 40^{\prime} \\ & \text { E101} \end{aligned}$ | $\begin{aligned} & \text { S01º } 40^{\prime} \\ & \text { E0970. } \end{aligned}$ | $\begin{aligned} & \hline \text { N01̊} 40^{\prime} \\ & \text { E097o } 07^{\prime} \end{aligned}$ | $\begin{aligned} & \hline \text { S01} 40^{\prime} \\ & \text { E101 }{ }^{\circ} 40^{\prime} \end{aligned}$ | 0 | 1 | 0 | 0 |
| 4278 | 61 | The main advantage of a remote indicating compass over a direct reading compass is that it: | requires less maintenance | is able to magnify the earth's magnetic field in order to attain greater accuracy | senses, rather than seeks, the magnetic meridian | has less moving parts | 0 | 0 | 1 | 0 |


| 4279 | 61 | Which of the following statements conceming the aircraft positions indicated on a triple fit Inertial Navigation System (INS)/ Inertial Reference System (IRS) on the CDU is correct? | The positions will be the same because they are an average of three different positions | The positions will only differ if one of the systems has been decoupled because of a detected malfunction | The positions will only differ if an error has been made when inputting the present position at the departure air port | The positions are likely to differ because they are calculated from different sour ces | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4280 | 61 | Which of the following statements conceming the operation of an Inertial Navigation System (INS)/Inertial Reference System (IRS) is correct? | NAV mode must be selected prior to movement of the aircraft off the gate | NAV mode must be selected on the runway just prior to take-off | NAV mode must be selected prior to the loading of passengers and/or freight | NAV mode must be selected when the alignment procedure is commenced | 1 | 0 | 0 | 0 |
| 4281 | 61 | Which of the following statements conceming the alignment procedure for Inertial Navigation Systems(INS)/Inertial Reference Systems (IRS) at mid-latitudes is correct? | INS/IRS can only be aligned in NAV mode | INS/IRS can be aligned in either the ALIGN or NAV mode | INS/IRS can only be aligned in the ALIGN mode | INS/IRS can be aligned in either the ALIGN or ATT mode | 0 | 1 | 0 | 0 |
| 4282 | 61 | The alignment time, at mid-latitudes, for an Inertial Reference System using laser ring gyros is approximately: | 5 MIN | 10 MIN | 20 MIN | 2 MIN | 0 | 1 | 0 | 0 |
| 4283 | 61 | What is the name given to an Inertial Reference System (IRS) which has the gyros and accelerometers as part of the unit's fixture to the aircraft structure? | Solid state | Ring laser | Strapdown | Rigid | 0 | 0 | 1 | 0 |
| 4284 | 61 | The sensors of an INS measure: | precession | acceleration | velocity | the horizontal component of the earth's rotation | 0 | 1 | 0 | 0 |
| 4285 | 61 | A pilot accidently turning OFF the INS in flight, and then tums it back ON a few moments later. Following this incident: | the INS is usable in NAV MODE after a position update | it can only be used for attitude reference | no useful information can be obtained from the INS | everything retums to normal and is usable | 0 | 1 | 0 | 0 |
| 4286 | 61 | The chart that is generally used for navigation in polar areas is based on a: | Direct Mercator projection | Gnomonic projection | Lambert conformal projection | Stereographic al projection | 0 | 0 | 0 | 1 |
| 4287 | 61 | (For this question use annex 061-9438A) <br> Complete line 2 of the 'FLIGHT NAVIGATION LOG', positions 'C' to 'D'. | $\begin{aligned} & \text { HDG } 193^{\circ}- \\ & \text { ETA } 1239 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 188^{\circ} \\ & \text { ETA } 1229 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 193^{\circ} \\ & \text { ETA } 1249 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & \text { HDG } 183^{\circ} \\ & \text { ETA } 1159 \\ & \text { UTC } \end{aligned}$ | 1 | 0 | 0 | 0 |
| 4288 | 61 | Position A is located on the equat or at longitude $130^{\circ} 00 \mathrm{E}$. <br> Position B is located 100 NM from A on a bearing of $225^{\circ}(\mathrm{T})$. <br> The coordinates of position $B$ are: | $\begin{aligned} & 01^{\circ} 11^{\prime} \mathrm{N} \\ & 128^{\circ} 49^{\prime} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 01^{\circ} 11^{\prime} \mathrm{S} \\ & 128^{\circ} 49^{\prime} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 01^{\circ} 11^{\prime} \mathrm{N} \\ & 131^{\circ} 11^{\prime} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 01^{\circ} 11 \text { 'S } \\ & 131^{\circ} 11^{\prime} \mathrm{E} \end{aligned}$ | 0 | 1 | 0 | 0 |
| 4289 | 61 | In order to fly from position $\mathrm{A}\left(10^{\circ} 00^{\prime} \mathrm{N}, 030^{\circ} 00^{\prime} \mathrm{W}\right)$ to position B ( $30^{\circ} 00^{\prime} \mathrm{N}, 050^{\circ} 00^{\prime} \mathrm{W}$ ), maintaining a constant true course, it is necessary to fly: | the great-circle route | a straight line plotted on a Lambert chart | a rhumb line track | the constant average drift route | 0 | - | 1 | 0 |
| 4290 | 61 | The rhumb line track between position $\mathrm{A}\left(45^{\circ} 00^{\prime} \mathrm{N}\right.$, $\left.010^{\circ} 00^{\prime} \mathrm{W}\right)$ and position $\mathrm{B}\left(48^{\circ} 30^{\prime} \mathrm{N}, 015^{\circ} 00^{\prime} \mathrm{W}\right)$ is approximately: | 345 | 315 | 330 | 300 | 0 | 1 | 0 | 0 |
| 4291 | 61 | The diameter of the Earth is approximately: | 40000 km | 12700 km | 6350 km | 18500 km | 0 | 1 | 0 | 0 |
| 4292 | 61 | (For this question refer to annex 061-12624A) <br> Which aeronautical chart symbol indicates an uncontrolled | 3 | 4 | 5 | 2 | 0 | 1 | 0 | 0 |


| 4293 | 61 | The nominal scale of a Lambert conformal conic chart is the: | scale at the equator | scale at the standard parallels | mean scale between pole and equator | mean scale between the parallels of the secant cone | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4294 | 61 | (For this question refer to annex 061-12625A) <br> Which aeronautical chart symbol indicates the boundary of | 2 | 3 | 4 | 5 | 0 | 0 | 0 | 1 |
| 4295 | 61 | A Mercator chart has a scale at the equator $=1: 3704000$. <br> What is the scale at latitude $60^{\circ} \mathrm{S}$ ? | 1:3208 000 | 1:185200 | 1:1852000 | 1:7408000 | 0 | 0 | 1 | 0 |
| 4296 | 61 | The distance measured between two points on a navigation map is 42 mm (millimetres). The scale of the chart is $1: 1600$ 000. <br> The actual distance between these two point is | 370.00 NM | 67.20 NM | 3.69 NM | 36.30 NM | 0 | 0 | 0 | 1 |
| 4297 | 61 | The standard parallels of a Lambert's conical orthomomhic projection are $07^{\circ} 40^{\prime} \mathrm{N}$ and $38^{\circ} 20^{\prime} \mathrm{N}$. | 0.42 | 0.39 | 0.60 | 0.92 | 0 | 1 | 0 | 0 |
| 4298 | 61 | On a Lambert conformal conic chart the convergence of the meridians: | is zero throughout the chart | varies as the secant of the latitude | equals earth convergency at the standard parallels | is the same as earth convergency at the parallel of origin | 0 | - | - | 1 |
| 4299 | 61 | A straight line drawn on a chart measures 4.63 cm and represents 150 NM. | 1:6000 000 | 1:3000 000 | 1:5000 000 | 1:1000 000 | 1 | 0 | 0 | 0 |
| 4300 | 61 | On a Polar Stereographic chart, the initial great circle course from $\mathrm{A} 70^{\circ} \mathrm{N} 060^{\circ} \mathrm{W}$ to $\mathrm{B} 70^{\circ} \mathrm{N} 060^{\circ} \mathrm{E}$ is approximately: | $030^{\circ}(\mathrm{T})$ | $330^{\circ}(\mathrm{T})$ | $150^{\circ}$ (T) | $210^{\circ}(\mathrm{T})$ | 1 | 0 | 0 | 0 |
| 4301 | 61 | The maximum difference between geocentric and geodetic latitude occurs at about: | $90^{\circ}$ North and South | $0^{\circ}$ North and South (equator) | $45^{\circ}$ North and South | $60^{\circ}$ North and South | 0 | 0 | 1 | 0 |
| 4302 | 61 | (For this question refer to annex 061-12632A) <br> Which aeronautical chart symbol indicates a group of lighted | 9 | 10 | 11 | 12 | 0 | 0 | 0 | 1 |
| 4303 | 61 | A course of $120^{\circ}(\mathrm{T})$ is drawn between ' $\mathrm{X}^{\prime}\left(61^{\circ} 30^{\prime} \mathrm{N}\right)$ and $\mathrm{Y}^{\prime}$ ( $58^{\circ} 30^{\prime} \mathrm{N}$ ) on a Lambert Conformal conic chart with a scale of $1: 1000000$ at $60^{\circ} \mathrm{N}$. <br> The chart distance between ' X ' and ' Y ' is: | 66.7 cm | 33.4 cm | 38.5 cm | 36.0 cm | 1 | 0 | - | 0 |
| 4304 | 61 | (For this question refer to annex 061-12638A) <br> Which aeronautical chart symbol indicates a lightship? | 14 | 16 | 10 | 12 | 0 | 1 | 0 | 0 |
| 4305 | 61 | (For this question refer to annex 061-12637A) <br> Which aeronautical chart symbol indicates an aeronautical | 15 | 16 | 10 | 14 | 1 | 0 | 0 | 0 |
| 4306 | 61 | (For this question refer to annex 061-12636A) <br> What is the meaning of aeronautical chart symbol No. 16 ? | Shipwreck showing above the surface at low tide | Off-shore lighthouse | Lightship | Off-shore helicopter landing platform | 0 | 0 | 1 | - |
| 4307 | 61 | (For this question refer to annex 061-12635A) <br> What is the meaning of aeronautical chart symbol No. 15 ? | Hazard to aerial navigation | Lighthouse | Aeronautical ground light | Visual reference point | 0 | 0 | 1 | 0 |
| 4308 | 61 | Given: value for the ellipticity of the Earth is $1 / 297$. <br> Earth's semi-major axis, as measured at the equator, equals 6378.4 km . | 6378.4 | 6367.0 | 6399.9 | 6356.9 | 0 | 0 | 0 | 1 |
| 4309 | 61 | (For this question refer to annex 061-12633A) <br> Which aeronautical chart symbol indicates an exceptionally | 9 | 11 | 13 | 14 | 0 | 0 | 1 | 0 |
| 4310 | 61 | On a Lambert Conformal Conic chart great circles that are not meridians are: | curves concave to the pole of projection | straight lines within the standard parallels | curves concave to the parallel of origin | straight lines regardless of distance | 0 | 0 | 1 | - |
| 4311 | 61 | (For this question refer to annex 061-12631A) <br> Which aeronautical chart symbol indicates a group of | 9 | 11 | 12 | 13 | 0 | 1 | 0 | 0 |


| 4312 | 61 | (For this question refer to annex 061-12630A) <br> Which aeronautical chart symbol indicates a lighted | 9 | 10 | 11 | 12 | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4313 | 61 | (For this question refer to annex 061-12629A) <br> Which aeronautical chart symbol indicates an unlighted | 12 | 9 | 10 | 11 | 0 | 1 | 0 | 0 |
| 4314 | 61 | (For this question refer to annex 061-12628A) <br> Which aeronautical chart symbol indicates a Way-point? | 15 | 6 | 7 | 8 | 0 | 0 | 0 | 1 |
| 4315 | 61 | (For this question refer to annex 061-12627A) <br> Which aeronautical chart symbol indicates a compulsory | 8 | 15 | 6 | 7 | 0 | 0 | 0 | 1 |
| 4316 | 61 | (For this question refer to annex 061-12626A) <br> Which aeronautical chart symbol indicates a non-compulsory | 15 | 6 | 7 | 8 | 0 | 1 | 0 | 0 |
| 4317 | 61 | (For this question refer to annex 061-12634A) <br> Which aeronautical chart symbol indicates an exceptionally | 14 | 10 | 12 | 13 | 1 | 0 | 0 | 0 |
| 4318 | 61 | What is the longitude of a position 6 NM to the east of $58^{\circ} 42^{\prime} \mathrm{N} 094^{\circ} 00^{\prime} \mathrm{W}$ ? | 09353.1 ${ }^{\text {W }}$ | 094¹2.0'W | 093048.5'W | 09354.0'W | 0 | 0 | 1 | 0 |
| 4319 | 61 | Given: $\begin{aligned} & \text { True Heading }=090^{\circ} \\ & \text { TAS }=180 \mathrm{kt} \\ & \text { GS }=180 \mathrm{kt} \end{aligned}$ | $360^{\circ} / 15 \mathrm{kt}$ | 190 $/ 15 \mathrm{kt}$ | 010 $/ 15 \mathrm{kt}$ | $180^{\circ} / 15 \mathrm{kt}$ | 1 | 0 | 0 | 0 |
| 4320 | 61 | Given: $\begin{aligned} & \text { True Heading }=090^{\circ} \\ & \text { TAS }=200 \mathrm{kt} \end{aligned}$ | 180 kt | 200 kt | 220 kt | 230 kt | 0 | 0 | 1 | 0 |
| 4321 | 61 | An aeroplane is flying at TAS 180 kt on a track of $090^{\circ}$. <br> The W/V is $045^{\circ} / 50 \mathrm{kt}$. <br> How far can the aeroplane fly out from its base and return in annhoim | 85 NM | 88 NM | 56 NM | 176 NM | 1 | 0 | 0 | 0 |
| 4322 | 61 | The following information is displayed on an Inertial Navigation System: <br> GS 520 kt , <br> True HDG $090^{\circ}$, <br> Drift angle $5^{\circ}$ right, | $220^{\circ} / 60 \mathrm{kt}$ | $325^{\circ} / 60 \mathrm{kt}$ | $320^{\circ} / 60 \mathrm{kt}$ | $225^{\circ} / 60 \mathrm{kt}$ | 0 | 0 | 1 | 0 |
| 4323 | 61 | The reported surface wind from the Control Tower is $240^{\circ} / 35$ kt. Runway $30\left(300^{\circ}\right)$. | 30 kt | 24 kt | 27 kt | 21 kt | 1 | 0 | 0 | 0 |
| 4324 | 61 | On a Direct Mercator chart, a rhumb line appears as a: | small circle concave to the nearer pole | spiral curve | curve convex to the nearer pole | straight line | 0 | 0 | 0 | 1 |
| 4325 | 61 | A great circle track joins position A (59 ${ }^{\circ}$ S $\left.141^{\circ} \mathrm{W}\right)$ and B ( $61^{\circ} \mathrm{S} 148^{\circ} \mathrm{W}$ ). <br> What is the difference between the great circle track at $A$ | It increases by $6^{\circ}$ | It decreases by $6^{\circ}$ | It increases by $3^{\circ}$ | It decreases by $3^{\circ}$ | 1 | 0 | 0 | 0 |
| 4326 | 61 | Given: $\begin{aligned} & \text { True Heading }=180^{\circ} \\ & \text { TAS }=500 \mathrm{kt} \end{aligned}$ | 435 kt | 600 kt | 535 kt | 450 kt | 1 | - | 0 | 0 |
| 4327 | 61 | A pilot receives the following signals from a VOR DME station: <br> radial $180^{\circ}+/-1^{\circ}$, distance $=200 \mathrm{NM}$. | +/- 2 NM | +/-7 NM | +/- 3.5 NM | +/-1 NM | 0 | 0 | 1 | 0 |
| 4328 | 61 | An aircraft is maintaining a $5.2 \%$ gradient is at 7 NM from the runway, on a flat terrain; its height is approximately: | 3640 FT | 2210 FT | 680 FT | 1890 FT | 0 | 1 | 0 | 0 |


| 4329 | 61 | A useful method of a pilot resolving, during a visual flight, any uncertainty in the aircraft's position is to maintain visual contact with the ground and: | fly the reverse of the heading being flown prior to becoming uncertain until a pinpoint is obtained | fly expanding circles untila pinpoint is obtained | fly reverse headings and associat ed timings until the point of departure is regained | set heading towards a line feature such as a coastline, motoway, river or railway | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4330 | 61 | (For this question use annex 061-12405A) <br> Which of the following beacons is 185 NM from AKRABERG | $\begin{array}{\|l} \hline \text { KIRKWALL } \\ \text { (N5858 W } \\ 00254) \\ \hline \end{array}$ | $\begin{aligned} & \hline \text { STORNOWA } \\ & \text { Y (N5815 } \\ & \text { W00617) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { SUMBURGH } \\ & \text { (N5955 } \\ & \text { W001 15) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { SAXAVORD } \\ & \text { (N6050 } \\ & \text { W00050) } \\ & \hline \end{aligned}$ | 0 | 0 |
| 4331 | 61 | (For this question use annex 061-12404A) <br> An aircraft on radial $110^{\circ}$ at a range of 120 NM from an vavinon vad (manen unnnnenl in nt manitinn. | $\begin{aligned} & \mathrm{N} 6127 \\ & \mathrm{~W} 00443 \end{aligned}$ | $\begin{array}{\|l\|} \hline N 6010 \\ \text { E00255 } \end{array}$ | $\begin{aligned} & \hline \text { N6109 } \\ & \text { E00255 } \end{aligned}$ | $\begin{aligned} & \mathrm{N} 6027 \\ & \mathrm{E} 00307 \end{aligned}$ | 0 | 0 |
| 4332 | 61 | (For this question use annex 061-12403A) <br> An aircraft on radial $315^{\circ}$ at a range of 150 NM from $\qquad$ | $\begin{aligned} & \hline \text { N6320 } \\ & \text { W01205 } \end{aligned}$ | $\begin{aligned} & \hline \text { N6020 } \\ & \text { W00405 } \end{aligned}$ | $\begin{aligned} & \hline \text { N6345 } \\ & \text { W01125 } \end{aligned}$ | $\begin{aligned} & \mathrm{N} 6040 \\ & \mathrm{~W} 00320 \end{aligned}$ | 1 | 0 |
| 4333 | 61 | An aircraft passes position $\mathrm{A}\left(60^{\circ} 00^{\prime} \mathrm{N} 120^{\circ} 00^{\prime} \mathrm{W}\right)$ on route to position $\mathrm{B}\left(60^{\circ} 00^{\prime} \mathrm{N} 140^{\circ} 30^{\prime} \mathrm{W}\right)$. <br> What is the great circle track on departure from A ? | $279{ }^{\circ}$ | $288^{\circ}$ | $261^{\circ}$ | $270^{\circ}$ | 1 | 0 |
| 4334 | 61 | Given the following: <br> True track: $192^{\circ}$ <br> Magnetic variation: $7^{\circ} \mathrm{E}$ <br> Drift angle: $5^{\circ}$ left | $180^{\circ}$ | $190^{\circ}$ | $194^{\circ}$ | $204^{\circ}$ | 0 | 1 |
| 4335 | 61 | An aircraft equipped with an Inertial Navigation System (INS) flies with INS 1 coupled with autopilot 1 . Both inertial navigation systems are navigating from way-point A to B. <br> The inertial systems' Central Display Units (CDU) sho shows: <br> - XTK on INS $1=0$ <br> - XTK on INS $2=8 \mathrm{~L}$ <br> (XTK = cross track) | only inertial navigation system No. 1 is drifting | the auto pilot is unserviceabl e in NAV mode | at least one of the inertial navigat on systems is drifting | only inertial navigation system No. 2 is drifting | 0 | 0 |
| 4336 | 61 | On a direct Mercator projection, at latitude $45^{\circ}$ North, a certain length represents 70 NM . <br> At latitude $30^{\circ}$ North, the same length represents | 57 NM | 70 NM | 81 NM | 86 NM | 0 | 0 |
| 4337 | 61 | Given: <br> Position A $45^{\circ} \mathrm{N}, ?^{\circ} \mathrm{E}$ <br> Position B $45^{\circ} \mathrm{N}, 45^{\circ} 15^{\prime} \mathrm{E}$ <br> Distance A-B = 280 NM | $38^{\circ} 39^{\prime} \mathrm{E}$ | $49^{\circ} 57^{\prime \prime} \mathrm{E}$ | $51^{\circ} 51{ }^{\prime} \mathrm{E}$ | $4^{\circ} 33^{\prime} \mathrm{E}$ | 1 | 0 |
| 4338 | 61 | On a polar stereog raphic projection chart showing the South Pole, a straight line joins position $\mathrm{A}\left(70^{\circ} \mathrm{S} 065^{\circ} \mathrm{E}\right)$ to position B ( $70^{\circ} \mathrm{S} 025^{\circ} \mathrm{W}$ ). <br> The true course on departure from position $A$ is | $315^{\circ}$ | $225^{\circ}$ | $250^{\circ}$ | $135^{\circ}$ | 0 | 1 |
| 4339 | 61 | On a direct Mercator projection, the distance measured between two meridians spaced $5^{\circ}$ apart at latitude $60^{\circ} \mathrm{N}$ is 8 cm . <br> The scale of this chart at latitude $60^{\circ} \mathrm{N}$ is approximately: | 1:4750 000 | 1:7000 000 | 1:6000 000 | 1:3500 000 | 0 | 0 |
| 4340 | 61 | Two positions plotted on a polar stereog raphic chart, A $\left(80^{\circ} \mathrm{N} 000^{\circ}\right)$ and $\mathrm{B}\left(70^{\circ} \mathrm{N} 102^{\circ} \mathrm{W}\right.$ ) are joined by a straight line whose highest latitude is reached at $035^{\circ} \mathrm{W}$. <br> At point $B$, the true course is: | $023^{\circ}$ | $247^{\circ}$ | $305^{\circ}$ | $203^{\circ}$ | 0 | - |
| 4341 | 61 | If an aeroplane was to circle around the Earth following parallel $60^{\circ} \mathrm{N}$ at a ground speed of 480 kt . In order to circle around the Earth along the equator in the same amount of time, it should fly at a ground speed of: | 240 kt | 550 kt | 480 kt | 960 kt | 0 | 0 |


| 4342 | 61 | \|Given: <br> Magnetic heading $311^{\circ}$ <br> Drift angle $10^{\circ}$ left <br> Relative bearing of NDB $270^{\circ}$ | 208 ${ }^{\circ}$ | $211^{\circ}$ | $180^{\circ}$ | $1221^{\circ}$ | 0 | 0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4343 | 61 | Given: <br> True heading $=310^{\circ}$ $\begin{aligned} & \text { TAS }=200 \mathrm{kt} \\ & \text { GS }=176 \mathrm{kt} \end{aligned}$ | 090 / 33 kt | $180^{\circ} / 33 \mathrm{kt}$ | $270^{\circ} / 33 \mathrm{kt}$ | $360^{\circ} / 33 \mathrm{kt}$ | 0 | ¢ | 0 |
| 4344 | 61 | Given the following: <br> Magnetic heading: $060^{\circ}$ <br> Magnetic variation: $8^{\circ} \mathrm{W}$ | 048 ${ }^{\circ}$ | $072^{\circ}$ | $056^{\circ}$ | $064^{\circ}$ | 0 | 01 | 0 |
| 4345 | 61 | An aircraft is following a true track of $048^{\circ}$ at a constant TAS of 210 kt . <br> The wind velocity is $350^{\circ} / 30 \mathrm{kt}$. | $\begin{aligned} & 192 \mathrm{kt}, 7^{\circ} \\ & \text { right } \end{aligned}$ | $\begin{aligned} & 200 \mathrm{kt}, 3.5^{\circ} \\ & \text { right } \end{aligned}$ | $192 \mathrm{kt}, 7^{\circ} \mathrm{left}$ | $225 \mathrm{kt}, 7^{\circ} \mathrm{left}$ | 1 | 0 | 0 |
| 4346 | 61 | Given: <br> FL 350, <br> Mach 0.80, <br> OAT $-55^{\circ} \mathrm{C}$. | $\begin{aligned} & 461 \mathrm{kt}, \text { LSS } \\ & 296 \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 461 \mathrm{kt}, \text { LSS } \\ & 576 \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 237 \mathrm{kt}, \mathrm{LSS} \\ & 296 \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 490 \mathrm{kt}, \text { LSS } \\ & 461 \mathrm{kt} \end{aligned}$ | - | 1-1 | - |
| 4347 | 61 | For a given track the: <br> Wind component $=+45 \mathrm{kt}$ <br> Drift angle $=15^{\circ}$ left | -35 kt | -65 kt | -55 kt | -45 kt | 0 | 10 | 0 |
| 4348 | 61 | Given: $\begin{aligned} & \text { Magnetic heading }=255^{\circ} \\ & \text { VAR }=40^{\circ} \mathrm{W} \\ & \text { GS }=375 \mathrm{kt} \end{aligned}$ | $16^{\circ}$ right | $7^{\circ}$ left | $7^{\circ}$ right | $9^{\circ}$ left | 0 | 1-1 | 0 |
| 4349 | 61 | The great circle distance between position $\mathrm{A}\left(59^{\circ} 34.1^{\mathrm{N}} \mathrm{N}\right.$ $\left.008^{\circ} 08.4^{\prime} \mathrm{E}\right)$ and $\mathrm{B}\left(30^{\circ} 25.9^{\prime} \mathrm{N} 171^{\circ} 51.6^{\prime} \mathrm{W}\right)$ is: | 2700 NM | 10800 NM | 5400 NM | 10800 km | 0 | 0 | 0 |
| 4350 | 61 | On a Mercator chart, the scale: | is constant throughout the chart | varies as $1 / 2$ cosine of the co-latitude | varies as <br> 1/cosine of <br> latitude <br> (1/cosine= <br> secant) | varies as the sine of the latitude | 0 | - | 0 |
| 4351 | 61 | Given: <br> Distance $A$ to $B=120 N M$, <br> After 30 NM aircraft is 3 NM to the left of course. | $8^{\circ}$ night | $6^{\circ}$ night | $4^{\circ}$ night | $8^{\circ}$ left | 1 | 0 | 0 |
| 4352 | 61 | Given:  <br> Distance 'A' to 'B' 1973 NM <br> Groundspeed 'out' 430 kt <br> Groundspeed 'back' 385 kt | 130 MIN | 145 MIN | 162 MIN | 181 MIN | 1 | 0 | 0 |
| 4353 | 61 | An aircraft was over ' $Q$ ' at 1320 hours flying direct to ' $R$ '. Given: | 1510 NM | 2290 NM | 2370 NM | 1310 NM | 0 | 1 |  |



| 4364 | 61 | The main reason for mounting the detector unit of a remote reading compass in the wingtip of an aeroplane is: | to ensure that the unit is in the most accessi ble position on the aircraft for ease of maintenance | by having detector units on both wingt ips, to cancel out the deviation effects caused by the aircraft strucure | to minimise the amount of deviation caused by aircraft magnetism and electrical circ uits | to maximise the units exposure to the earth's magnetic field | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4365 | 61 | Route 'A' ( $44^{\circ} \mathrm{N} 026^{\circ} \mathrm{E}$ ) to 'B' ( $46^{\circ} \mathrm{N} 024^{\circ} \mathrm{E}$ ) forms an angle of $35^{\circ}$ with longitude $026^{\circ} \mathrm{E}$. Average magnetic variation between ' $\mathrm{A}^{\prime}$ and ' B ' is $3^{\circ} \mathrm{E}$. <br> What is the average magnetic course from ' A ' to ' B '? | 038 ${ }^{\circ}$ | $322^{\circ}$ | $328^{\circ}$ | 032 ${ }^{\circ}$ | 0 | 1 | 0 |
| 4366 | 61 | An aircraft was over 'A' at 1435 hours flying direct to ' $B$ '. | 2844 NM | 2141 NM | 1611 NM | 1759 NM | 0 | 1 | 0 |
| 4367 | 61 | An aircraft is planned to fly from position 'A' to position ' B ', distance 480 NM at an average GS of 240 kt . It departs 'A' at 1000 UTC. <br> After flying 150 NM along track from ' A ', the aircraft is 2 MIN behind planned time. <br> Usina the actual GS experienced. what is the revised ETA at | 1157 | 1206 | 1203 | 1153 | - | 1-1 | 0 |
| 4368 | 61 | (For this question use annex 061-12402A) <br> What are the initial true course and distance between nnnitinnn MIK Onn MIntonn and MIEEn | $\begin{array}{\|rc} \hline 032^{\circ} & - \\ 470 \mathrm{NM} \end{array}$ | $\begin{array}{rc} \hline 036^{\circ} & - \\ 638 & \mathrm{NM} \end{array}$ | $\begin{array}{rr} \hline 029^{\circ} & - \\ 570 \mathrm{NM} \end{array}$ | $\begin{array}{rc} \hline 042^{\circ}- \\ 635 \mathrm{NM} \end{array}$ | 0 | 1-1 | 0 |
| 4369 | 61 | Given: <br> Distance ' A ' to ' B ' is 100 NM, <br> Fix obtained 40 NM along and 6 NM to the left of course. <br> What heading alteration must be made to reach 'B'? | $18^{\circ}$ Right | $15^{\circ}$ Right | $9^{\circ}$ Right | $6^{\circ}$ Right | 0 | 1 | 0 |
| 4370 | 61 | Given: <br> Distance ' A ' to ' B ' is 325 NM , <br> Planned GS 315 kt , <br> ATD 1130 UTC, | 375 kt | 395 kt | 335 kt | 355 kt | - | - | 0 |
| 4371 | 61 | Given: <br> Distance ' A ' to ' B ' is 475 NM, <br> Planned GS 315 kt , <br> ATD 1000 UTC, | 340 kt | 360 kt . | 300 kt | 320 kt . | 1 | 0 | 0 |
| 4372 | 61 | Given: <br> Magnetic track $=210^{\circ}$, <br> Magnetic HDG $=215^{\circ}$, $\operatorname{VAR}=15^{\circ} \mathrm{E}$ | 235\% $/ 50 \mathrm{kt}$ | $300^{\circ} / 30 \mathrm{kt}$ | 265\%/50 kt | 195\% 50 kt | 0 | 0 | 10 |
| 4373 | 61 | Given: $\begin{aligned} & \text { Magnetic track }=075^{\circ}, \\ & \\ & \mathrm{HDG}=066^{\circ}(\mathrm{M}) \\ & \operatorname{VAR}=11^{\circ} \mathrm{E} \end{aligned}$ | $180 \%$ \% kt | $340 \% 45 \mathrm{kt}$ | $320 \%$ k kt | 210\%/15 kt | 0 |  |  |



| 4387 | 61 | (For this question use annex 061-12559A) <br> What is the radialand DME distance from CON VOR/DME (N5354.8 W00849.1) to position N5340 W00820? | $\begin{array}{lll} 311^{\circ}-22 \\ N M & & \\ \hline \end{array}$ | $\begin{array}{lll} 240^{\circ}-24 \\ N M & & \end{array}$ | $\begin{aligned} & 140^{\circ}-23 \\ & N M \end{aligned}$ | $\begin{array}{ll} 119^{\circ}-42 \\ N M & \end{array}$ | 0 | 0 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4388 | 61 | (For this question use annex 061-12558A) <br> What is the radial and DME distance from CON VOR/DME (N5354.8 W00849.1) to position N5400 W00800? | $\begin{array}{ll} 320^{\circ}-8 \\ N M & \end{array}$ | $\begin{array}{lll} 094^{\circ}-64 \\ N M & & \end{array}$ | $\begin{array}{lll} 260^{\circ}-30 \\ N M & & \end{array}$ | $\begin{array}{lll} \hline 088^{\circ}-29 \\ N M & \end{array}$ | 0 | 0 | 0 | 1 |
| 4389 | 61 | (For this question use annex 061-12557A) <br> What is the radial and DME distance from CON VOR/DME (N5354.8 W00849.1) to position N5430 W00900? | $\begin{aligned} & 214^{\circ}-26 \\ & \text { NM } \end{aligned}$ | O49 NM | $\begin{array}{lll} 169^{\circ}-35 \\ N M & & \end{array}$ | $\begin{array}{ll} 358^{\circ}-36 \\ N M & \end{array}$ | 0 | 0 | 0 | 1 |
| 4390 | 61 | An aircraft at latitude $10^{\circ}$ North flies south at a groundspeed of $445 \mathrm{~km} / \mathrm{HR}$. | 0350'S | 0200'S | 12¹5'S | $22^{\circ} 00^{\prime} \mathrm{S}$ | 0 | 1 | 0 | 0 |
| 4391 | 61 | (For this question use annex 061-12555A) <br> What is the radialand DME distance from SHA VOR/DME (N5243.3 W00853.1) to position N5220 W00810? | $\begin{aligned} & 132^{\circ}-36 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 212^{\circ}-26 \\ & N M \end{aligned}$ | $\begin{array}{ll} 139^{\circ}-35 \\ \text { NM } & \end{array}$ | $\begin{array}{ll} 129^{\circ}-46 \\ N M & \end{array}$ | 0 | 0 | 1 | 0 |
| 4392 | 61 | (For this question use annex 061-12563A) <br> What is the radial and DME distance from BEL VOR/DME (N5439.7 W00613.8) to position N5500 W00700? | $\begin{aligned} & 296^{\circ}-65 \\ & N M \end{aligned}$ | $\begin{aligned} & 126^{\circ}-33 \\ & \mathrm{NM} \end{aligned}$ | $\begin{aligned} & 222^{\circ}-48 \\ & \text { NM } \end{aligned}$ | $\begin{array}{lll} \hline 315^{\circ}-34 \\ \text { NM } & & \end{array}$ | 0 | 0 | 0 | 1 |
| 4393 | 61 | (For this question use annex 061-12553A) <br> What is the radialand DME distance from SHA VOR/DME (N5243.3 W00853.1) to position N5300 W00940? | $\begin{aligned} & 309^{\circ}-33 \\ & N M \end{aligned}$ | $\begin{array}{lll} 057^{\circ}-27 \\ N M & & \end{array}$ | $\begin{aligned} & 293^{\circ}-33 \\ & \text { NM } \end{aligned}$ | $\begin{array}{lll} 324^{\circ}-17 \\ N M & & \end{array}$ | 1 | - | 0 | 0 |
| 4394 | 61 | (For this question use annex 061-12552A) <br> What is the radialand DME distance from CRK VOR/DME (N5150.4 W00829.7) to position N5140 W00730? | $\begin{array}{ll} 293^{\circ}-39 \\ N M & \end{array}$ | $\begin{aligned} & 106^{\circ}-38 \\ & N M \end{aligned}$ | $\begin{array}{ll} 113^{\circ}-38 \\ \text { NM } & \\ \hline \end{array}$ | $\begin{array}{ll} 104^{\circ}-76 \\ N M & \end{array}$ | 0 | - | 1 | 0 |
| 4395 | 61 | (For this question use annex 061-12551A) <br> What is the radial and DME distance from CRK VOR/DME (N5 150.4 W00829.7) to position N5230 W00750? | $\begin{array}{ll} 023^{\circ}-48 \\ \text { NM } & \end{array}$ | $\begin{array}{lll} 017^{\circ}-43 \\ \text { NM } & \end{array}$ | $\begin{array}{lll} 039^{\circ}-48 \\ N M & \end{array}$ | $\begin{aligned} & 024^{\circ}-43 \\ & \text { NM } \end{aligned}$ | 0 | 0 | 1 | - |
| 4396 | 61 | (For this question use annex 061-12550A) <br> What is the radial and DME distance from CRK VOR/DME (N5 150.4 W00829.7) to position N5210 W00920? | $\begin{array}{ll} 350^{\circ}-22 \\ N M & \end{array}$ | $\begin{aligned} & 295^{\circ}-38 \\ & N M \end{aligned}$ | $\begin{aligned} & 170^{\circ}-22 \\ & \text { NM } \end{aligned}$ | $\begin{array}{ll} 311^{\circ}-38 \\ N M & \end{array}$ | 0 | 0 | 0 | 1 |
| 4397 | 61 | (For this question use annex 061-12549A) <br> What is the radial and DME distance from CRK VOR/DME (N5150.4 W00829.7) to position N5220 W00810? | $\begin{aligned} & 014^{\circ}-33 \\ & N M \end{aligned}$ | $\begin{array}{ll} 220^{\circ}-40 \\ N M & \end{array}$ | $\begin{aligned} & 030^{\circ}-33 \\ & \mathrm{NM} \end{aligned}$ | $\begin{aligned} & 048^{\circ}-40 \\ & N M \end{aligned}$ | 0 | - | 1 | 0 |
| 4398 | 61 | (For this question use annex 061-9437A) <br> Complete line 1 of the 'FLIGHT NAVIGATIONLOG'; positions 'A' to 'B'. | $\begin{aligned} & 268^{\circ}-1114 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & 282^{\circ}-1128 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & 282^{\circ}-1114 \\ & \text { UTC } \end{aligned}$ | $\begin{aligned} & 268^{\circ}-1128 \\ & \text { UTC } \end{aligned}$ | 1 | 0 | 0 | 0 |
| 4399 | 61 | (For this question use annex 061-12556A) <br> What is the radial and DME distance from SHA VOR/DME (N5243.3 W00853.1) | $\begin{array}{lll} 354^{\circ}-34 \\ N M \end{array}$ | $\begin{array}{ll} 198^{\circ}-37 \\ N M & \end{array}$ | $\begin{array}{lll} 346^{\circ}-34 \\ N M & \end{array}$ | $\begin{array}{lll} 214^{\circ}-37 \\ N M & & \end{array}$ | 0 | 0 | 0 | 1 |
| 4400 | 61 | On a Direct Mercator chart at latitude of $45^{\circ} \mathrm{N}$, a certain length represents a distance of 90 NM on the earth. <br> The same length on the chart will represent on the earth, at latitude $30^{\circ} \mathrm{N}$, a distance of : | 110 NM | 73.5 NM | 78 NM | 45 NM | 1 | 0 | 0 | 0 |
| 4401 | 61 | The 'departure' between positions $60^{\circ} \mathrm{N} 160^{\circ} \mathrm{E}$ and $60^{\circ} \mathrm{N}$ ' x ' is 900 NM . | $170^{\circ} \mathrm{W}$ | $140^{\circ} \mathrm{W}$ | $145^{\circ} \mathrm{E}$ | $175^{\circ} \mathrm{E}$ | 1 | 0 | 0 | 0 |
| 4402 | 61 | An aircraft at position $60^{\circ} \mathrm{N} 005^{\circ} \mathrm{W}$ tracks $090^{\circ}(\mathrm{T})$ for 315 km . On completion of the flight the longitude will be: | 002 ${ }^{\circ} 10^{\prime} \mathrm{W}$ | 000o15'E | 00040'E | 005¹5'E | 0 | 0 | 1 | 0 |
| 4403 | 61 | A flight is to be made from ' A ' $49^{\circ} \mathrm{S} 180^{\circ} \mathrm{E} / \mathrm{W}$ to ' B ' $58^{\circ} \mathrm{S}$, $180^{\circ} \mathrm{E} / \mathrm{W}$. <br> The distance in kilometres from ' A ' to ' B ' is approximately: | 540 | 804 | 1000 | 1222 | 0 | 0 | 1 | 0 |
| 4404 | 61 | At what approximate date is the earth furthest from the sun (aphelion)? | End of December | Beginning of January | End of September | Beginning of July | 0 | 0 | 0 | 1 |
| 4405 | 61 | At what approximate date is the earth closest to the sun (perihelion)? | Beginning of January | End of March | Beginning of July | End of June |  | 0 | 0 | 0 |


| 4406 | 61 | Assuming mid-latitudes $\left(40^{\circ}\right.$ to $\left.50^{\circ} \mathrm{N} / \mathrm{S}\right)$. <br> At which time of year is the relationship between the length of day and night, as well as the rate of change of declination of the sun, changing at the greatest rate? | Spring equinox and autumn equinox | Summer solstice and spring equinox | summer solstice and winter solstice | Winter solstice and autumn equinox | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4407 | 61 | Two points $A$ and $B$ are 1000 NM apart. TAS $=490 \mathrm{kt}$. <br> On the flight between $A$ and $B$ the equivalent headwind is -20 kt. <br> On the retum leg between $B$ and $A$, the equivalent headwind is +40 kt . <br> What distance from $A$. alona the route $A$ to $B$. is the the Point | 470 NM | 455 NM | 500 NM | 530 NM | 0 | 0 |
| 4408 | 61 | In which two months of the year is the difference between the transit of the Apparent Sun and Mean Sun across the Greenwich Meridian the greatest? | June and December | April and August | February and November | March and September | 0 | 0 |
| 4409 | 61 | (For this question use annex 061-12562A) <br> What is the radialand DME distance from BEL VOR/DME (N5439.7 W00613.8) to position N5440 W00730? | $\begin{array}{ll} 098^{\circ}-45 \\ N M & \end{array}$ | $\begin{aligned} & 278^{\circ}-44 \\ & \text { NM } \end{aligned}$ | $\begin{array}{lll} 090^{\circ}-46 \\ N M & \end{array}$ | $\begin{array}{lll} \hline 278^{\circ}-10 \\ N M & \end{array}$ | 0 | 1 |
| 4410 | 61 | On a Direct Mercator chart at latitude $15^{\circ} \mathrm{S}$, a certain length represents a distance of 120 NM on the earth. <br> The same length on the chart will represent on the earth, at latitude $10^{\circ} \mathrm{N}$, a distance of : | 124.2 NM | 118.2 NM | 122.3 NM | 117.7 NM | 0 | 0 |
| 4411 | 61 | (For this question use annex 061-12567A) <br> What is the average track ( ${ }^{\circ} \mathrm{M}$ ) and distance between WTD NDB (N521 1.3 W00705.0) and BAL VOR (N5318.0 | $\begin{array}{ll} \hline 206^{\circ}-71 \\ N M & \end{array}$ | $\begin{aligned} & 198^{\circ}-72 \\ & \text { NM } \end{aligned}$ | $\begin{array}{ll} 026^{\circ}-71 \\ \text { NM } & \end{array}$ | $\begin{array}{lll} 018^{\circ}-153 \\ \text { NM } & \end{array}$ | 0 | 0 |
| 4412 | 61 | (For this question use annex 061-12566A) <br> What is the average track ( ${ }^{\circ} \mathrm{M}$ ) and distance between CRN NDB (N5318.1 W00856.5) and WTD NDB (N5211.3 | $\begin{array}{ll} 135^{\circ}-96 \\ \text { NM } & \\ \hline \end{array}$ | $\begin{aligned} & 322^{\circ}-95 \\ & N M \end{aligned}$ | $\begin{array}{lll} \hline 142^{\circ}-95 \\ N M & & \end{array}$ | $\begin{array}{lll} 315^{\circ}-94 \\ N M & & \end{array}$ | 0 | 0 |
| 4413 | 61 | (For this question use annex 061-12565A) <br> What is the average track ( ${ }^{\circ} \mathrm{M}$ ) and distance between CRK VOR (N5150.4 W00829.7) and CRN NDB (N5318.1 | $\begin{aligned} & 177^{\circ}-92 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 357^{\circ}-89 \\ & N M \end{aligned}$ | $\begin{array}{ll} 169^{\circ}-91 \\ N M & \end{array}$ | $\begin{array}{ll} 349^{\circ}-90 \\ N M & \end{array}$ | 0 | 1 |
| 4414 | 61 | (For this question use annex 061-12564A) <br> What is the average track ( ${ }^{\circ} \mathrm{M}$ ) and distance between WTD NDB (N521 1.3 W00705.0) and KER NDB (N52 10.9 | $\begin{aligned} & 090^{\circ}-91 \\ & \mathrm{NM} \end{aligned}$ | $\begin{aligned} & 270^{\circ}-89 \\ & \text { NM } \end{aligned}$ | $\begin{aligned} & 098^{\circ}-90 \\ & N M \end{aligned}$ | $\begin{aligned} & 278^{\circ}-90 \\ & N M \end{aligned}$ | 0 | 0 |
| 4415 | 61 | Given: <br> Direct Mercator chart with a scale of 1:200000 at equator; <br> Chart length from ' A ' to ' B ', in the vicinity of the equator, 11 cm. | 12 NM | 21 NM | 22 NM | 14 NM | 1 | 0 |
| 4416 | 61 | What is the highest latitude listed below at which the sun will reach an altitude of $90^{\circ}$ above the horizon at some time during the year? | $0^{\circ}$ | $23^{\circ}$ | $45^{\circ}$ | $66^{\circ}$ | 0 | 1 |
| 4417 | 61 | What is the meaning of the term "standard time" ? | It is the time zone system applicable only in the USA | It is an expression for local mean time | It is another term for UTC | It is the time set by the legal authorities for a country or part of a country | 0 | 0 |
| 4418 | 61 | Given: <br> The coordinates of the heliport at Issy les Moulineaux are: $N 48^{\circ} 50^{\prime} E 002^{\circ} 16.5^{\prime}$ | S4110' <br> W177ํ.43.5' | $\begin{aligned} & \mathrm{S} 41^{\circ} 10^{\prime} \\ & \mathrm{E} 177^{\circ} 43.5^{\prime} \end{aligned}$ | $\begin{aligned} & \text { S48ํ050' } \\ & \text { W177̊ㄴ3. } 5^{\prime} \end{aligned}$ |  | 0 | 0 |
| 4419 | 61 | How many NM would an aircraft travel in 1 MIN 45 SEC if GS is 135 kt ? | 2.36 | 3.25 | 39.0 | 3.94 | 0 | 0 |
| 4420 | 61 | Given: <br> Course $040^{\circ}(\mathrm{T})$, <br> TAS is 120 kt , <br> Wind speed 30 kt . | $120^{\circ}$ | $130^{\circ}$ | $145^{\circ}$ | $115^{\circ}$ |  |  |


| 4421 | 61 | Given: <br> IAS 120 kt, <br> FL 80, | 120 kt | 132 kt | 141 kt | 102 kt | 0 | 0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4422 | 61 | Given: <br> Compass Heading $090^{\circ}$, <br> Deviation $2^{\circ} \mathrm{W}$, <br> Variation $12^{\circ} \mathrm{E}$, <br> TAS 160 kt. <br> Whilst maintaining a radial $070^{\circ}$ from a VOR station, | $340 \% / 25 \mathrm{kt}$ | $340 \% 98 \mathrm{kt}$ | 155\%/25 kt | $160 \%$ \% kt | 0 | 0 |  |
| 4423 | 61 | Given: <br> Pressure Altitude 29000 FT, <br> のnt rion | 27500 FT | 31000 FT | 33500 FT | 26000 FT | 1 | 0 |  |
| 4424 | 61 | Given: <br> M 0.80, <br> OAT $-50^{\circ} \mathrm{C}$, <br> FL 330, <br> GS 490 kt, | 025\%/45 kt | 020\%/95 kt | 025\%/47 kt | 200\%/95 kt | 0 | 1 |  |
| 4425 | 61 | Given: <br> TAS 487kt, <br> FL 330, | 0.76 | 0.78 | 0.81 | 0.84 | 0 | 0 |  |
| 4426 | 61 | What is the ISA temperature value at FL 330? | $-56^{\circ} \mathrm{C}$ | $-66^{\circ} \mathrm{C}$ | $-81^{\circ} \mathrm{C}$ | $-50^{\circ} \mathrm{C}$ | 0 | 0 |  |
| 4427 | 61 | When an aircraft on a westerly heading on the northern hemisphere accelerates, the effect of the acceleration error causes the magnetic compass to: | lag behind the tuming rate of the aircraft | indicate a tum towards the south | to turn faster than the actual tuming rate of the aircraft | indicate a tum towards the north | 0 | 0 |  |
| 4428 | 61 | When is the magnetic compass most effective? | In the region of the magnetic North Pole. | On the geographic equator | About midway betw een the magnetic poles | In the region of the magnetic South Pole. | 0 | - | 0 |
| 4429 | 61 | Given: $\text { TAS = } 472 \text { kt, }$ <br> True HDG $=005^{\circ}$, | $7^{\circ} \mathrm{R}-487 \mathrm{kt}$ | $6^{\circ} \mathrm{L}-487 \mathrm{kt}$ | $7{ }^{\circ} \mathrm{R}-491 \mathrm{kt}$ | 7º - 491 kt | 0 | 1 | 0 |
| 4430 | 61 | What is the local meantime, position $65^{\circ} 25^{\prime} \mathrm{N} 123^{\circ} 45$ 'W at 2200 UTC? | 2200 | 0615 | 0815 | 1345 | 0 | 0 |  |
| 4431 | 61 | An aircraft flies the following rhumb line tracks and distances from position $04^{\circ} 00^{\prime} \mathrm{N} 030^{\circ} 00^{\prime} \mathrm{W}$ : <br> 600 NM South, <br> then 600 NM East, <br> then 600 NM North, | $\begin{array}{l\|} 04^{\circ} 00^{\prime} \mathrm{N} \\ 030^{\circ} 00^{\prime} \mathrm{W} \end{array}$ | $\begin{aligned} & 03^{\circ} 58^{\prime} \mathrm{N} \\ & 030^{\circ} 02^{\prime} \mathrm{W} \end{aligned}$ | $\begin{aligned} & 04^{\circ} 00^{\prime} \mathrm{N} \\ & 029^{\circ} 58^{\prime} \mathrm{W} \end{aligned}$ | $\begin{aligned} & 04^{\circ} 00^{\prime} \mathrm{N} \\ & 030^{\circ} 02^{\prime} \mathrm{W} \end{aligned}$ | - | - | 0 |
| 4432 | 61 | Isogrives are lines that connect positions that have: | the same variation | $\mathrm{O}^{\circ}$ magnetic dip | the same grivation | the same horizontal magnetic field strength | - | 0 | 0 |
| 4433 | 61 | An aircraft flies a great circle track from $56^{\circ} \mathrm{N} 070^{\circ} \mathrm{W}$ to $62^{\circ}$ N $110^{\circ} \mathrm{E}$. | 1788 NM | 2040 NM | 3720 NM | 5420 NM | 0 | 0 | 0 |
| 4434 | 61 | An aircraft travels 2.4 statute miles in 47 seconds. <br> What is its groundspeed? | 209 kt | 131 kt | 160 kt | 183 kt | 0 | 0 | 0 |
| 4435 | 61 | How long will it take to fly 5 NM at a groundspeed of 269 Kt ? | $\begin{aligned} & \hline 0 \mathrm{MIN} 34 \\ & \text { SEC } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1 \mathrm{MIN} 07 \\ & \text { SEC } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1 \text { MIN } 55 \\ & \text { SEC } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2 \text { MIN } 30 \\ & \text { SEC } \\ & \hline \end{aligned}$ | 0 | 1 |  |


| 4436 | 61 | $730 \mathrm{FT} / \mathrm{MIN}$ equals: | $5.2 \mathrm{~m} / \mathrm{sec}$ | $1.6 \mathrm{~m} / \mathrm{sec}$ | $2.2 \mathrm{~m} / \mathrm{sec}$ | $3.7 \mathrm{~m} / \mathrm{sec}$ | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4437 | 61 | 265 US-GAL equals? (Specific gravity 0.80) | 862 kg | 895 kg | 940 kg | 803 kg | 0 | 0 | 0 | 1 |
| 4438 | 61 | Given: $\begin{aligned} & \text { TAS = } 140 \mathrm{kt}, \\ & \text { True HDG }=302^{\circ}, \end{aligned}$ | $9^{\circ} \mathrm{R}-143 \mathrm{kt}$ | $9^{\circ} \mathrm{L}-146 \mathrm{kt}$ | $18^{\circ} \mathrm{R}-146 \mathrm{kt}$ | $16^{\circ} \mathrm{L}-156 \mathrm{kt}$ | 0 | 0 | 0 | 1 |
| 4439 | 61 | Given: $\text { TAS = } 290 \mathrm{kt} \text {, }$ <br> True HDG $=171^{\circ}$, | $4^{\circ} \mathrm{L}-314 \mathrm{kt}$ | $4^{\circ} \mathrm{R}-310 \mathrm{kt}$ | $4^{\circ} \mathrm{R}-314 \mathrm{kt}$ | $4^{\circ} \mathrm{L}-310 \mathrm{kt}$ | 1 | 0 | 0 | 0 |
| 4440 | 61 | Given: GS $=135 \mathrm{kt}$. <br> Distance from $A$ to $B=433 N M$. | 3 HR 20 MIN | 3 HR 12 MIN | 3 HR 25 MIN | 3 HR 19 MIN | 0 | 1 | 0 | 0 |
| 4441 | 61 | The angular difference, on a Lambert conformal conic chart, between the arrival and departure track is equal to: | difference in longitude | map convergence | earth convergence | conversion angle | 0 | 1 | 0 | 0 |
| 4442 | 61 | Given: <br> True course A to $B=250^{\circ}$ <br> Distance A to $\mathrm{B}=315 \mathrm{NM}$ $\text { TAS = } 450 \mathrm{kt} .$ | 0810 UTC | 0716 UTC | 0736 UTC | 0730 UTC | 0 | 0 | 1 | 0 |
| 4443 | 61 | An Agonic line is a line that connects: | positions that have $0^{\circ}$ variation | positions that have the same variation | points of equal magnetic dip | points of equal magnetic horizontal field strength | 1-1 | 0 | 0 | 0 |
| 4444 | 61 | Parallels of latitude, except the equator, are: | Rhumb lines | Great circles | both Rhumb lines and Great circles | are neither Rhumb lines nor Great circles | 1 | 0 | 0 | 0 |
| 4445 | 61 | Given: GS = 510 kt . <br> Distance $A$ to $B=43 \mathrm{NM}$ | 6 | 7 | 5 | 4 | 0 | 0 | 1 | 0 |
| 4446 | 61 | Given: <br> true track $070^{\circ}$ <br> variation $30^{\circ} \mathrm{W}$ <br> deviation $+1^{\circ}$ | 089 ${ }^{\circ}$ | $091^{\circ}$ | $100^{\circ}$ | $101^{\circ}$ | 1-1 | - | 0 | 0 |
| 4447 | 61 | The angle between True North and Magnetic North is called : | drift | variation | deviation | compass error | 0 | 1 | 0 | 0 |
| 4448 | 61 | Given: GS = 122 kt . <br> Distance from $A$ to $B=985 \mathrm{NM}$. | 8 HR 10 MIN | 8 HR 04 MIN | 7 HR 48 MIN | 7 HR 49 MIN | 0 | 1 | 0 | 0 |
| 4449 | 61 | What is the value of the magnetic dip at the magnetic south pole? | $0^{\circ}$ | $90^{\circ}$ | $45^{\circ}$ | $60^{\circ}$ | 0 | 1 | 0 | 0 |
| 4450 | 61 | Given: GS = 236 kt . <br> Distance from $A$ to $B=354 \mathrm{NM}$ | 1 HR 40 MIN | 1 HR 30 MIN | 1 HR 09 MIN | 1 HR 10 MIN | 0 | 1 | 0 | 0 |
| 4451 | 61 | Given: GS = 435 kt . <br> Distance from A to $B=1920 \mathrm{NM}$. | 4 HR 10 MIN | 4 HR 25 MIN | 3 HR 25 MIN | 3 HR 26 MIN | 0 | 1 | 0 | 0 |
| 4452 | 61 | Given: GS = 345 kt . <br> Distance from $A$ to $B=3560$ NM. | $\begin{aligned} & 11 \text { HR } 00 \\ & \text { MIN } \end{aligned}$ | $\begin{aligned} & 11 \text { HR } 02 \\ & \text { MIN } \end{aligned}$ | 10 HR 19 MIN | $\begin{aligned} & 10 \text { HR } 05 \\ & \text { MIN } \end{aligned}$ | 0 | 0 | 1 | 0 |
| 4453 | 61 | Given: GS = 480 kt . <br> Distance from $A$ to $B=5360 \mathrm{NM}$. | $11 \text { HR } 07$ <br> MIN | $11 \text { HR } 15$ <br> MIN | $11 \text { HR } 10$ $\mathrm{MIN}$ | $\begin{aligned} & 11 \text { HR } 06 \\ & \text { MIN } \end{aligned}$ | 0 | 0 | 1 | 0 |
| 4454 | 61 | Given: GS = 95 kt . <br> Distance from $A$ to $B=480 \mathrm{NM}$. | 5 HR 03 MIN | 4 HR 59 MIN | 5 HR 00 MIN | 5 HR 08 MIN | 1 | 0 | 0 | 0 |
| 4455 | 61 | Given: GS = 105 kt . <br> Distance from $A$ to $B=103 \mathrm{NM}$. | 00 HR 58 MIN | 01 HR 01 <br> MIN | 00 HR 59 MIN | $\begin{aligned} & 00 \text { HR } 57 \\ & \text { MIN } \end{aligned}$ | 0 | 0 | 1 | 0 |


| 4456 | 61 | Given: $\text { TAS = } 470 \mathrm{kt},$ <br> True HDG = $317^{\circ}$ | $3^{\circ} \mathrm{R}-470 \mathrm{kt}$ | 50 $\mathrm{L}-475 \mathrm{kt}$ | $5^{\circ} \mathrm{R}-475 \mathrm{kt}$ | 50 ${ }^{\circ}-470 \mathrm{kt}$ | 0 | 0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4457 | 61 | At a specific location, the value of magnetic variation: | depends on the type of compass installed | depends on the magnetic heading | depends on the true heading | varies slowly over time | 0 | 0 |  |
| 4458 | 61 | Given: $\text { TAS = } 270 \mathrm{kt},$ <br> True HDG = $270^{\circ}$, | 6L-256kt | 6R-251kt | 8R-259kt | 6R-259kt | 0 | 0 |  |
| 4459 | 61 | Given: <br> FL120, <br> OAT is ISA standard, <br> CAS is 200 kt , <br> Track is $222^{\circ}(\mathrm{M})$, | $\begin{aligned} & 065^{\circ}(\mathrm{T}) / 70 \\ & \mathrm{kt.} \end{aligned}$ | $\begin{aligned} & 050^{\circ}(\mathrm{T}) / 70 \\ & \mathrm{kt.} . \end{aligned}$ | $040^{\circ}(\mathrm{T}) / 105$ $\mathrm{kt} .$ | $\begin{aligned} & 055^{\circ}(\mathrm{T}) / 105 \\ & \mathrm{kt} . \end{aligned}$ | 0 | 1 | 0 |
| 4460 | 61 | At latitude $60^{\circ} \mathrm{N}$ the scale of a Mercator projection is $1: 5$ 000 000. The length on the chart between 'C' $\mathrm{N} 60^{\circ} \mathrm{E} 008^{\circ}$ and 'D' $\mathrm{N} 60^{\circ} \mathrm{W} 008^{\circ}$ is: | 16.2 cm | 35.6 cm | 19.2 cm | 17.8 cm | 0 | 0 |  |
| 4461 | 61 | Given : <br> A is $\mathrm{N} 55^{\circ} 000^{\circ}$ <br> $B$ is $\mathrm{N} 54^{\circ} \mathrm{E} 010^{\circ}$ <br> The average true course of the great circle is $100^{\circ}$. | 096 ${ }^{\circ}$ | $104^{\circ}$ | $107^{\circ}$ | $100^{\circ}$ | 0 | 0 |  |
| 4462 | 61 | Given: <br> Distance A to B is 360 NM. <br> Wind component A-B is -15 kt , <br> Wind component $\mathrm{B}-\mathrm{A}$ is +15 kt , | 180 NM | 170 NM | 165 NM | 195 NM | 0 | 0 | 0 |
| 4463 | 61 | Given: <br> Half way between two reporting points the navigation log gives the following information: <br> TAS 360 kt, <br> W/V 330 $/ 80 \mathrm{kt}$, <br> Compass heading $237^{\circ}$, | 373 kt | 360 kt | 403 kt | 354 kt | - | - | 0 |
| 4464 | 61 | (For this question use appendix ) <br> Given: <br> TAS is 120 kt . <br> ATA 'X' 1232 UTC, | 1302 UTC | 1257 UTC | 1300 UTC | 1303 UTC | 1 | 0 | 00 |
| 4465 | 61 | A negative (westerly) magnetic variation signifies that: | Compass North is East of Magnetic North | Compass <br> North is <br> West of <br> Magnetic <br> North | True North is East of Magnetic North | True North is West of Magnetic North | 0 | 0 | 1-10 |
| 4466 | 61 | In northern hemisphere, during an acceleration in an easterly direction, the magnetic compass will indicate: | a heading of East | a decrease in heading | an increase in heading | an apparent tum to the South | 0 | 1 | 0 |
| 4467 | 61 | Deviation applied to magnetic heading gives: | magnetic track | compass heading | true heading | magnetic course | 0 | 1 | 0 |
| 4468 | 61 | The purpose of compass check swing is to: | cancel out the horizontal component of the earth's magnetic field | cancel out the effects of the magnetic fields found on board the aeroplane | measure the angle between Magnetic North and Compass North | cancel out the vertical component of the earth's magnetic field |  | 0 |  |


| 4469 | 61 | At what approximate latitude is the length of one minute of arc along a meridian equal to one NM ( 1852 m ) correct? | $30^{\circ}$ | $45^{\circ}$ | $0^{\circ}$ | $190^{\circ}$ | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4470 | 61 | Isogonals are lines of equal : | wind velocity. | magnetic variation. | compass deviation | pressure. | 0 | 1 | 0 | 0 |
| 4471 | 61 | Given: GS = 120 kt . <br> Distance from $A$ to $B=84 \mathrm{NM}$. | $00 \text { HR } 43$ $\mathrm{MIN}$ | 00 HR 44 MIN | $\begin{aligned} & \hline 00 \text { HR } 45 \\ & \text { MIN } \end{aligned}$ | $\begin{aligned} & 00 \text { HR } 42 \\ & \text { MIN } \end{aligned}$ | 0 | 0 | 0 | 1 |
| 4472 | 61 | The distance between positions $A$ and $B$ is 180 NM . An aircraft departs position $A$ and after having travelled 60 NM, its position is pinpointed 4 NM left of the intended track. Assuming no change in wind velocity, what alteration of heading must be made in order to arrive at position B ? | $8^{\circ}$ Right | $2^{\circ}$ Left | $4^{\circ}$ Right | $6^{\circ}$ Right | 0 | 0 | 0 | 1 |
| 4473 | 61 | An aircraft at FL290 is required to commence descent when 50 NM from a VOR and to cross that VOR at FL80. <br> Mean GS during descent is 271 kt . <br> What is the minimum rate of descent required? | $1800 \mathrm{FT} / \mathrm{MIN}$ | $1900 \mathrm{FT} / \mathrm{MIN}$ | $2000 \mathrm{FT} / \mathrm{MIN}$ | $1700 \mathrm{FT} / \mathrm{MIN}$ | 0 | 1 | 0 | - |
| 4474 | 61 | Given: <br> Magnetic track $=315^{\circ}$, <br> $H D G=301^{\circ}(\mathrm{M})$, <br> $V A R=5^{\circ} \mathrm{W}$, | 190 \% /63 kt | $355 \% 15 \mathrm{kt}$ | 195\%61 kt | $195 \% 63 \mathrm{kt}$ | 1 | 0 | 0 | - |
| 4475 | 61 | Assuming zero wind, what distance will be covered by an aircraft descending 15000 FT with a TAS of 320 kt and maintaining a rate of descent of $3000 \mathrm{FT} / \mathrm{MIN}$ ? | 16.0 NM | 26.7 NM | 19.2 NM | 38.4 NM | 0 | 1 | 0 | 0 |
| 4476 | 61 | A Lambert conformal conic chart has a constant of the cone of 0.80 . <br> A straight line course drawn on this chart from $\mathrm{A}\left(53^{\circ} \mathrm{N}\right.$ $004^{\circ} \mathrm{W}$ ) to $B$ is $080^{\circ}$ at $A$; course at $B$ is $092^{\circ}(T)$. <br> What ic the Innoitudo of $R$ ? | $011^{\circ} \mathrm{E}$ | 00933'E | 008E | 0190E | 1 | 0 | - | - |
| 4477 | 61 | Given: <br> Runway direction $305^{\circ}(\mathrm{M})$, <br>  | 21 kt | 24 kt | 27 kt | 18 kt | 1 | 0 | 0 | 0 |
| 4478 | 61 | An aircraft at FL350 is required to commence descent when 85 NM from a VOR and to cross the VOR at FL80. The mean GS for the descent is 340 kt . <br> What is the minimum rate of descent required? | $1800 \mathrm{FT} / \mathrm{MIN}$ | $1900 \mathrm{FT} / \mathrm{MIN}$ | $1600 \mathrm{FT} / \mathrm{MIN}$ | $1700 \mathrm{FT} / \mathrm{MIN}$ | 1 | 0 | 0 | 0 |
| 4479 | 61 | An island is observed by weather radar to be $15^{\circ}$ to the left. <br> The aircraft heading is $120^{\circ}(\mathrm{M})$ and the magnetic variation $17^{\circ} \mathrm{W}$. <br> What is the true bearing of the aircraft from the island? | 088 ${ }^{\circ}$ | $122^{\circ}$ | $268^{\circ}$ | $302^{\circ}$ | 0 | 0 | 1 | - |
| 4480 | 61 | During a low level flight 2 parallel roads that are crossed at right angles by an aircraft. The time between these roads can be used to check the aircraft: | drift | groundspeed | position | track | 0 | 1 | 0 | 0 |
| 4481 | 61 | Given: <br> FL250, <br> OAT $-15^{\circ} \mathrm{C}$, | 0.44 | 0.39 | 0.40 | 0.42 | 0 | 0 | 1 | 0 |
| 4482 | 61 | Given: $\text { TAS = } 220 \text { kt; }$ <br> Magnetic course $=212^{\circ}$, | 290 kt | 246 kt | 250 kt | 186 kt | 0 | 0 | 0 | 1 |
| 4483 | 61 | An aircraft travels 100 statute miles in 20 MIN , how long does it take to travel 215 NM ? | 90 MIN | 80 MIN | 50 MIN | 100 MIN | 0 | 0 | 1 | 0 |
| 4484 | 61 | Given: $\text { TAS = } 485 \text { kt, }$ <br> True HDG $=226^{\circ}$, | $9^{\circ} \mathrm{R}-533 \mathrm{kt}$ | $7^{\circ} \mathrm{R}-531 \mathrm{kt}$ | $9^{\circ} \mathrm{R}-433 \mathrm{kt}$ | $8^{\circ} \mathrm{L}-435 \mathrm{kt}$ |  | 10 | 0 | 0 |


| 4485 | 61 | Which of the following statements conceming earth magnetism is completely correct? | An isogonal is a line which connects places of equal dip; the aclinic is the line of zero magnetic dip | An isogonal is a line which connects places with the same magnetic variation; the aclinic connects places with the same magnetic field strength | An isogonal is a line which connects places with the same magnetic variation; the aclinic is the line of zero magnetic dip | An isogonal is a line which connects places with the same magnetic variation; the agonic line is the line of zero magnetic dip | 0 | 01 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4486 | 61 | Given: <br> Chart scale is $1: 1850000$. <br> The chart distance between two points is 4 centimetres. | 40 NM | 74 NM | 100 NM | 4 NM | 1 | 00 | 0 |
| 4487 | 61 | The Earth can be considered as being a magnet with the: | red pole near the north pole of the earth and the direction of the magnetic force pointing strai ght down to the earth's surface | blue pole near the north pole of the earth and the direction of the magnetic force pointing strai ght up from the earth's surface | red pole near the north pole of the earth and the direction of the magnetic force pointing strai ght up from the earth's surface | blue pole near the north pole of the earth and the direction of the magnetic force pointing strai ght down to the earth's surface | 0 | (1) |  |
| 4488 | 61 | Complete the following statement regarding magnetic variation. <br> The charted values of magnetic variation on earth normally change annually due to: | magnetic pole moveme nt causing numerical values at all locations to increase or decrease | magnetic pole moveme nt causing numerical values at all locations to increase. | a reducing field strength causing numerical values at all locations to decrease. | an increasing field strength causing numerical values at all locations to increase. | 1 | ¢ | 0 |
| 4489 | 61 | Which one of the following is an advantage of a remote reading compass as compared with a standby compass? | It eliminates the effect of tuming and acceleration errors by pendulously suspending the detector unit | It is more reliable because it is operated electrically and power is always available from sources withi n the aircraft | It senses the magnetic meridian instead of seeking it, increasing compass sensitivity | It is lighter than a direct reading compass because it employs, apart from the detector unit, existing aircraft equipment | 0 | 01 | 0 |
| 4490 | 61 | Which of the following statements is correct concerning the effect of turning errors on a direct reading compass? | Turning errors are greatest on east/west headings, and are greatest at high latitudes | Turning errors are greatest on north/south headings, and are greatest at high latitudes | Turning errors are greatest on east/west headings, and are least at high latitudes | Turning errors are greatest on north/south headings, and are least at high latitudes | 0 |  |  |


| 4491 | 61 | Which of the following is an occasion for carrying out a compass swing on a Direct Reading Compass? | Before an aircraft goes on any flight that involves a large change of magnetic latitude | After any of the aircraft radio equipment has been changed due to unserviceabil ity | Whenever an aircraft carries a large freight load regardless of its content | After an aircraft has passed through a severe electrical stom, or has been struck by lightning | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4492 | 61 | The parallels on a Lambert Conformal Conic chart are represented by: | straight lines | parabolic lines | hyperbolic lines | arcs of concentric circles | 0 | 0 |
| 4493 | 61 | The main reason that day and night, throughout the year, have different duration, is due to the: | inclination of the ecliptic to the equator | earth's rotation | relative speed of the sun along the ecliptic | gravitational effect of the sun and moon on the speed of rotation of the earth | 1 | 0 |
| 4494 | 61 | An aircraft departing $\mathrm{A}\left(\mathrm{N} 40^{\circ} 00^{\prime} \mathrm{E} 080^{\circ} 00^{\prime}\right)$ flies a constant true track of $270^{\circ}$ at a ground speed of 120 kt . <br> What are the coordinates of the position reached in 6 HR ? | $\begin{aligned} & \mathrm{N} 40^{\circ} 00^{\prime} \\ & \mathrm{E} 068^{\circ} 10^{\prime} \end{aligned}$ | $\begin{aligned} & \mathrm{N} 40^{\circ} 00^{\prime} \\ & \mathrm{E} 064^{\circ} 20^{\prime} \end{aligned}$ | $\begin{aligned} & \mathrm{N} 40^{\circ} 00^{\prime} \\ & \mathrm{E} 070^{\circ} 30^{\prime} \end{aligned}$ | $\begin{aligned} & \mathrm{N} 40^{\circ} 00^{\prime} \\ & \mathrm{E} 060^{\circ} 00^{\prime} \end{aligned}$ | 0 | 1 |
| 4495 | 61 | The lines on the earth's surface that join points of equal magnetic variation are called: | isogrives | isoclines | isogonals | isotachs | 0 | 0 |
| 4496 | 61 | An island appears $30^{\circ}$ to the left of the centre line on an airbome weather radar display. What is the true bearing of the aircraft from the island if at the time of observation the aircraft was on a magnetic heading of $276^{\circ}$ with the magnetic variation $12^{\circ} \mathrm{W}$ ? | $234^{\circ}$ | 038 ${ }^{\circ}$ | 054 ${ }^{\circ}$ | $318^{\circ}$ | 0 | 0 |
| 4497 | 61 | At the magnetic equator, when accelerating after take off on heading West, a direct reading compass : | underreads the heading | indicates a tum to the south | indicates the correct heading | overreads the heading | 0 | 0 |
| 4498 | 61 | The ICAO definition of ETA is the: | actual time of arrival at a point or fix | estimated time of arrival at an en-route point or fix | estimated time en route | estimated time of arrival at destination | 0 | 0 |
| 4499 | 61 | An aircraft at FL350 is required to descend to cross a DME facility at FL80. <br> Maximum rate of descent is $1800 \mathrm{FT} / \mathrm{MIN}$ and mean GS for descent is 276 kt . <br> The minimum ranne from the RNF at whinh decenent chnold | 69 NM | 79 NM | 49 NM | 59 NM | 1 | 0 |
| 4500 | 61 | Given: $\begin{aligned} & \text { TAS = } 190 \mathrm{kt}, \\ & \text { True HDG }=085^{\circ}, \end{aligned}$ | $4^{\circ} \mathrm{L}-145 \mathrm{kt}$ | $8^{\circ} \mathrm{L}-146 \mathrm{kt}$ | $7^{\circ} \mathrm{L}-156 \mathrm{kt}$ | $4^{\circ} \mathrm{L}-168 \mathrm{kt}$ | 0 | 1 |
| 4501 | 61 | The term drift refers to the wander of the axis of a gyro in: | the vertical and horizontal plane | any plane | the horizontal plane | the vertical plane | 0 | 0 |
| 4502 | 61 | An aircraft at FL370 is required to commence descent when 100 NM from a DME facility and to cross the station at FL1 20. <br> If the mean GS during the descent is 396 kt , the minimum rate of descent required is approximately: | 1650 FT/MIN | $2400 \mathrm{FT} / \mathrm{MIN}$ | $1000 \mathrm{FT} / \mathrm{MIN}$ | $1550 \mathrm{FT} / \mathrm{MIN}$ | 1 | 0 |
| 4503 | 61 | An aircraft at FL140, IAS 210 kt , OAT $-5^{\circ} \mathrm{C}$ and wind component minus 35 kt , is required to reduce speed in order to cross a reporting point 5 MIN later than planned. <br> Assuming that flight conditions do not change, when 150 NM from the reporting point the IAS should be reduced by: | 15 kt | 20 kt | 25 kt | 30 kt | 0 | 1 |
| 4504 | 61 | An aircraft at FL370 is required to commence descent at 120 NM from a VOR and to cross the facility at FL130. If the mean GS for the descent is 288 kt , the minimum rate of descent required is: | 860 FT/MIN | 890 FT/MIN | 920 FT/MIN | 960 FT/MIN | 0 | 0 |


| 4505 | 61 | An aircraft at FL310, M0.83, temperature $-30^{\circ} \mathrm{C}$, is required to reduce speed in order to cross a reporting point five minutes later than planned. <br> Assuming that a zero wind component remains unchanged, when 360 NM from the reporting point Mach Number should | M0.74 | M0.76 | M0.78 | M0.80 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4506 | 61 | A Lambert conformal conic chart has a constant of the cone of 0.75 . <br> The initial course of a straight line track drawn on this chart from $A\left(40^{\circ} \mathrm{N} 050^{\circ} \mathrm{W}\right)$ to $B$ is $043^{\circ}(\mathrm{T})$ at $A$; course at $B$ is 055 ${ }^{\circ}(\mathrm{T})$. | $34^{\circ} \mathrm{W}$ | $36^{\circ} \mathrm{W}$ | $38^{\circ} \mathrm{W}$ | $41^{\circ} \mathrm{W}$ | 1 | 0 | 0 |
| 4507 | 61 | Given: <br> Runway direction $210^{\circ}(\mathrm{M})$, <br> C.infonn ininノ nonornnionlt | 19 kt | 16 kt | 13 kt | 10 kt | 0 | 0 | 01 |
| 4508 | 61 | At 0422 an aircraft at FL370, GS 320kt, <br> is on the direct track to VOR'X' 185 NM distant. <br> The aircraft is required to cross VOR ' X ' at FL80. <br> For a mean rate of descent of $1800 \mathrm{FT} / \mathrm{MIN}$ at a mean GS of 232 kt , | 0451 | 0454 | 0445 | 0448 | 0 | 0 | 10 |
| 4509 | 61 | An aircraft at FL330 is rerquired to commence descent when 65 NM from a VOR and to cross the VOR at FL100. The mean GS during the descent is 330 kt . <br> What is the minimum rate of descent required? | 1850 FT/MIN | 1950 FT/MIN | 1650 FT/MIN | $1750 \mathrm{FT} / \mathrm{MIN}$ | 0 | 1 | 0 |
| 4510 | 61 | An aircraft obtains a relative bearing of $315^{\circ}$ from an NDB at 0830. At 0840 the relative bearing from the same position is $270^{\circ}$. <br> Assuming no drift and a GS of 240 kt , what is the | 60 NM | 30 NM | 40 NM | 50 NM | 0 | 0 | 10 |
| 4511 | 61 | The equivalent of $70 \mathrm{~m} / \mathrm{sec}$ is approximately: | 136 kt | 145 kt | 210 kt | 35 kt | 1 | 0 | 0 |
| 4512 | 61 | A ground feat ure was observed on a relative bearing of $325^{\circ}$ and five minutes later on a relative bearing of $280^{\circ}$. The aircraft heading was $165^{\circ}(\mathrm{M})$, variation $25^{\circ} \mathrm{W}$, drift $10^{\circ}$ Right and GS 360 kt . When the relative bearing was $280^{\circ}$, the distance and true bearing of the aircraft from the feature was: | $\begin{aligned} & 30 \mathrm{NM} \text { and } \\ & 060^{\circ} \end{aligned}$ | 30 NM and $240^{\circ}$ | $\begin{aligned} & 40 \mathrm{NM} \text { and } \\ & 110^{\circ} \end{aligned}$ | 40 NM and $290^{\circ}$ | 0 | - | 00 |
| 4513 | 61 | On a chart, the distance along a meridian between latitudes $45^{\circ} \mathrm{N}$ and $46^{\circ} \mathrm{N}$ is 6 cm . The scale of the chart is approximately: | 1:185000 | $\begin{aligned} & 1: 18500 \\ & 000 \end{aligned}$ | 1:1850 000 | 1:1000 000 | 0 | 0 | 10 |
| 4514 | 61 | An aircraft at FL120, IAS 200 kt , OAT $-5^{\circ}$ and wind component +30 kt , is required to reduce speed in order to cross a reporting point 5 MIN later than planned. <br> Assuming flight conditions do not change, when 100 NM from the reporting point IAS should be reduced to: | 174 kt | 159 kt | 165 kt | 169 kt | - | - | 00 |
| 4515 | 61 | Given: <br> Runway direction $083^{\circ}(\mathrm{M})$, <br>  | 27 kt | 31 kt | 34 kt | 24 kt | 0 | - | 01 |
| 4516 | 61 | Approximately how many nautical miles correspond to 12 cm on a map with a scale of 1:2000000? | 130 | 150 | 329 | 43 | 1 | 0 | 0 |
| 4517 | 61 | An aircraft at FL350 is required to cross a VOR/DME facility at <br> FL1 10 and to commence descent when 100 NM from the facility. <br> If the mean GS for the descent is 335 kt , the minimum rate | $1340 \mathrm{FT} / \mathrm{MIN}$ | 1390 FT/MIN | $1240 \mathrm{FT} / \mathrm{MIN}$ | 1290 FT/MIN | 1 | 0 | 0 |
| 4518 | 61 | An aircraft at FL370, M0.86, OAT $-44^{\circ} \mathrm{C}$, headwind component 110 kt , is required to reduce speed in order to cross a reporting point 5 MIN later than planned. <br> If the speed reduction were to be made 420 NM from the reporting point, what Mach Number is required? | M0.73 | M0.75 | M0.79 | M0.81 | 0 |  |  |


| 4519 | 61 | Given: <br> For take-off an aircraft requires a headwind component of at least 10 kt and has a cross-wind limitation of 35 kt . The angle between the wind direction and the runway is $60^{\circ}$, Calculate the minimum and maximum allowable wind speeds? | $\begin{aligned} & 18 \mathrm{kt} \text { and } \\ & 50 \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 20 \mathrm{kt} \text { and } 40 \\ & \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 12 \mathrm{kt} \text { and } \\ & 38 \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 15 \mathrm{kt} \text { and } \\ & 43 \mathrm{kt} \end{aligned}$ | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4520 | 61 | An aircraft at FL390 is required to descend to cross a DME facility at FL70. Maximum rate of descent is 2500 FT/MIN, mean GS during descent is 248 kt . What is the minimum range from the DME at which descent should commence? | 68 NM | 53 NM | 58 NM | 63 NM | 0 | 1 | 0 | 0 |
| 4521 | 61 | Given: <br> An aircraft is on final approach to runway $32 R\left(322^{\circ}\right)$; <br> The wind velocity reported by the tower is $350^{\circ} / 20 \mathrm{kt}$.; <br> TAS on approach is 95 kt . <br> In order to maintain the centre line, the aircraft's heading | $328^{\circ}$ | $322^{\circ}$ | $316^{\circ}$ | $326^{\circ}$ | 1 | 0 | 0 | 0 |
| 4522 | 61 | (For this question use annex 061-1829A and the data for 1300 UTC) <br> 1300 UTC DR position $37^{\circ} 30^{\prime} \mathrm{N} 021^{\circ} 30^{\prime} \mathrm{W}$ alter heading PORT SANTO NDB ( $33^{\circ} 03^{\prime} \mathrm{N} 016^{\circ}{ }^{\circ} 3^{\prime} \mathrm{W}$ ) <br> TAS 450 kt, | 1344 | 1341 | 1354 | 1348 | 0 | 0 | 0 | 1 |
| 4523 | 61 | What is the ratio between the litre and the US-GAL? | $\begin{array}{\|l} \hline 1 \text { US-GAL } \\ \text { equals } 4.55 \\ \text { litres } \\ \hline \end{array}$ | $\begin{aligned} & 1 \text { litre equals } \\ & \text { 4.55 US-GAL } \end{aligned}$ | $\begin{aligned} & 1 \text { US-GAL } \\ & \text { equals } 3.78 \\ & \text { litres } \end{aligned}$ | 1 litre equals 3.78 US-GAL | 0 | 0 | 1 | - |
| 4524 | 61 | The sensitivity of a direct reading compass varies: | inversely with the vertical component of the earth's magnetic field | directly with the horizontal co mponent of the earth's magnetic field | directly with the vertical component of the earth's magnetic field | inversely with both vertical and horizontal components of the earth's magnetic field | 0 | 1 | 0 | 0 |
| 4525 | 61 | What is the final position after the following rhumb line tracks and distances have been followed from position $60^{\circ} 00^{\prime} \mathrm{N}$ $030^{\circ} 00^{\prime} \mathrm{W}$ ? <br> South for 3600 NM, <br> East for 3600 NM, <br> North for 3600 NM. | $\begin{aligned} & 59^{\circ} 00^{\prime} \mathrm{N} \\ & 090^{\circ} 00^{\prime} \mathrm{W} \end{aligned}$ | $\begin{aligned} & 60^{\circ} 00^{\prime} \mathrm{N} \\ & 090^{\circ} 00^{\prime} \mathrm{W} \end{aligned}$ | $\begin{aligned} & 60^{\circ} 00^{\prime} \mathrm{N} \\ & 030^{\circ} 00^{\prime} \mathrm{E} \end{aligned}$ | $\begin{aligned} & 59^{\circ} 00^{\prime} \mathrm{N} \\ & 060^{\circ} 00^{\prime} \mathrm{W} \end{aligned}$ | 0 | 1-1 | 0 | - |
| 4526 | 61 | In an Inertial Navigation System (INS), Ground Speed (GS) is calculated: | from TAS and W/V from Air Data Comput er (ADC) | from TAS and W/V from RNAV data | by integrating gyro precession in N/S and E/W directions respectively | by integrating measured acceleration | 0 | 0 | 0 | 1 |
| 4527 | 61 | Given: $\begin{aligned} & \text { TAS }=375 \text { kt, } \\ & \text { True HDG }=124^{\circ}, \end{aligned}$ | 126-320 kt | $125-318$ kt | 123-320 kt | 125-322 kt | 0 | 0 | 1 | 0 |
| 4528 | 61 | Given: <br> true track $352^{\circ}$ <br> variation $11^{\circ} \mathrm{W}$ <br> deviation is $-5^{\circ}$ | $018^{\circ}$ | 025 ${ }^{\circ}$ | $358^{\circ}$ | $346^{\circ}$ | - | 0 | 1-1 | - |


| 4529 | 61 | Given : <br> True altitude 9000 FT, OAT $-32^{\circ} \mathrm{C}$, | 215 kt | 200 kt | 210 kt | 220 kt | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4530 | 61 | Given: <br> An aircraft is flying a track of $255^{\circ}(\mathrm{M})$, <br> 2254 UTC, it crosses radial $360^{\circ}$ from a VOR station, 2300 UTC, it crosses radial $330^{\circ}$ from the same station. At 2300 UTC, the distance between the aircraft and the | less than it was at 2254 UTC | the same as it was at 2254 UTC | greater than it was at 2254 UTC | randomly different than it was at 2254 UTC | 0 | 1 | - | 0 |
| 4531 | 61 | The distance between two waypoints is 200 NM, <br> To calculate compass heading, the pilot used $2^{\circ} \mathrm{E}$ magnetic variation instead of $2^{\circ} \mathrm{W}$. <br> Assuming that the forecast W/V applied, what will the off trank dictanmoho at the corned wavnoint? | 14 NM | 7 NM | 0 NM | 21 NM | 1 | 0 | 0 | 0 |
| 4532 | 61 | The scale on a Lambert conformal conic chart : | is constant along a meridian of longitude | is constant across the whole map | varies slightly as a function of latitude and longitude | is constant along a parallel of latitude | 0 | 0 | 0 | 1 |
| 4533 | 61 | 5 HR 20 MIN 20 SEC corre sponds to a longitude difference of: | $75^{\circ} 00$ | $78^{\circ} 45{ }^{\prime}$ | $8^{\circ} 05^{\prime}$ | $81^{\circ} 10$ | 0 | 0 | 1 | 0 |
| 4534 | 61 | The Local Mean Time at longitude $095^{\circ} 20^{\prime} \mathrm{W}$, at 0000 UTC, is : | $\begin{aligned} & 1738: 40 \\ & \text { same day } \end{aligned}$ | $\begin{aligned} & \text { 0621:20 } \\ & \text { same day } \end{aligned}$ | $\begin{aligned} & \hline 1738: 40 \\ & \text { previous day } \end{aligned}$ | 0621:20 previous day | 0 | 0 | 1 | 0 |
| 4535 | 61 | Isogonic lines connect positions that have: | the same angle of magnetic dip | the same variation | $0^{\circ}$ variation | the same elevation | 0 | 1 | 0 | 0 |
| 4536 | 61 | The circumference of the earth is approximately: | 10800 NM | 21600 NM | 43200 NM | 5400 NM | 0 | 1 | 0 | 0 |
| 4537 | 61 | Seasons are due to the: | Earth's rotation on its polar axis | variable distance between Earth and Sun | inclination of the polar axis with the ecliptic plane | Earth's elliptical orbit around the Sun | 0 | 0 | 1 | 0 |
| 4538 | 61 | Given: <br> TAS $=370 \mathrm{kt}$, <br> True HDG $=181^{\circ}$, | $189-370 \mathrm{kt}$ | 186-370 kt | 176-370 kt | 192-370 kt | 0 | 1 | 0 | 0 |
| 4539 | 61 | Civil twilight is defined by : | sun altitude is $12^{\circ}$ below the celestial horizon | sun altitude is $18^{\circ}$ below the celestial horizon | sun upper edge tangential to horizon | sun altitude is $6^{\circ}$ below the celestial horizon | 0 | - | - | -1 |
| 4540 | 61 | Given: $\text { TAS = } 125 \mathrm{kt},$ <br> True HDG $=355^{\circ}$, | 002-98 kt | 005-102 kt | 345-100 kt | 348-102 kt | 0 | 1 | - | - |
| 4541 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=135 \mathrm{kt}, \\ & \mathrm{HDG}\left({ }^{\circ} \mathrm{T}\right)=278, \end{aligned}$ | 283-150 kt | 279-152 kt | 282-148 kt | 275-150 kt | 1 | 0 | 0 | 0 |
| 4542 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=480 \mathrm{kt}, \\ & \mathrm{HDG}\left({ }^{\circ} \mathrm{T}\right)=040^{\circ}, \end{aligned}$ | 032-425 kt | 036-435 kt | 034-445 kt | 028-415 kt | 0 | - | 1 | - |
| 4543 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=155 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=216^{\circ}, \end{aligned}$ | 226-186 kt | 231-196 kt | 224-175 kt | 222-181 kt | 0 | 1 | - | - |
| 4544 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=170 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=100^{\circ}, \end{aligned}$ | 098-178 kt | 109-182 kt | 091-183 kt | 103-178 kt | - | 1-1 | 0 | - |


| 4545 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=235 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=076^{\circ} \end{aligned}$ | 5R - 207 kt | 77R-204 kt | 7L-269 kt | 5L-255 kt | 0 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4546 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=440 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=349^{\circ} \end{aligned}$ | 5L - 385 kt | 4L - 415 kt | 2L - 420 kt | 6L - 395 kt | 0 | 1 | 0 | 0 |
| 4547 | 61 | Given: <br> True course $300^{\circ}$ <br> drift $8^{\circ} \mathrm{R}$ <br> variation $10^{\circ} \mathrm{W}$ | $294^{\circ}$ | $278^{\circ}$ | $306^{\circ}$ | $322^{\circ}$ | 0 | 0 | 1 | 0 |
| 4548 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=465 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=124^{\circ}, \end{aligned}$ | 4L-400 kt | 6L - 400 kt | 8L - 415 kt | 3L - 415 kt | 0 | 0 | 1 | 0 |
| 4549 | 61 | Given: $\begin{aligned} & \text { TAS }=132 \mathrm{kt}, \\ & \text { True HDG }=257^{\circ} \end{aligned}$ | $3^{\circ} \mathrm{L}-166 \mathrm{kt}$ | $4{ }^{\circ} \mathrm{R}-165 \mathrm{kt}$ | $2^{\circ} \mathrm{R}-166 \mathrm{kt}$ | $4{ }^{\circ} \mathrm{L}-167 \mathrm{kt}$ | 0 | 1 | 0 | 0 |
| 4550 | 61 | Given: <br> True track $180^{\circ}$ <br> Drift $8^{\circ}$ R <br> Compass heading $195^{\circ}$ | $9^{\circ} \mathrm{W}$ | $21^{\circ} \mathrm{W}$ | $25^{\circ} \mathrm{W}$ | $5^{\circ} \mathrm{W}$ | 0 | 1 | - | - |
| 4551 | 61 | On a Mercator chart, at latitude $60^{\circ} \mathrm{N}$, the distance measured between W002 ${ }^{\circ}$ and $\mathrm{E} 008^{\circ}$ is 20 cm . The scale of this chart at latitude $60^{\circ} \mathrm{N}$ is approximately: | 1:2780 000 | 1:278000 | 1:5560 000 | 1:556000 | 1 | 0 | 0 | - |
| 4552 | 61 | An aircraft takes-off from an airport 2 hours before sunset. The pilot flies a track of $090^{\circ}(\mathrm{T})$, W/N $130^{\circ} / 20 \mathrm{kt}$, TAS 100 kt. In order to retum to the point of departure before sunset, the furthest distance which may be travelled is: | 115 NM | 105 NM | 84 NM | 97 NM | 0 | 0 | 0 | 1 |
| 4553 | 61 | Assume a Mercator chart. <br> The distance between positions $A$ and $B$, located on the same parallel and $10^{\circ}$ longitude apart, is 6 cm . The scale at the parallel is $1: 9260000$. | $60^{\circ} \mathrm{N}$ or S | $30^{\circ} \mathrm{N}$ orS | $0^{\circ}$ | $45^{\circ} \mathrm{N}$ orS | 1 | 0 | 0 | 0 |
| 4554 | 61 | On a Lambert chart (standard parallels $37^{\circ} \mathrm{N}$ and $65^{\circ} \mathrm{N}$ ), with respect to the straight line drawn on the map between A ( $\mathrm{N} 49^{\circ} \mathrm{W} 030^{\circ}$ ) and $\mathrm{B}\left(\mathrm{N} 48^{\circ} \mathrm{W} 040^{\circ}\right)$, the: | great circle and rhumb line are to the south | great circle and rhumb line are to the north | great circle is to the north, the rhumb line is to the south | rhumb line is to the north, the great circle is to the south | 1 | - | - | - |
| 4555 | 61 | A direct Mercator graticule is based on a projection that is : | spherical | concentric | cylindrical | conical | 0 | 0 | 1 | 0 |
| 4556 | 61 | Given: <br> Aircraft at FL 150 overhead an airport Elevation of aiport 720 FT. <br> QNH is 1003 hPa . | 14720 FT | 15280 FT | 15840 FT | 14160 FT | 0 | 1 | 0 | 0 |
| 4557 | 61 | An aircraft takes off from the ae rodrome of BRIOUDE (altitude 1483 FT , QFE $=963 \mathrm{hPa}$, temperature $=32^{\circ} \mathrm{C}$ ). <br> Five minutes later, passing 5000 FT on QFE, the second altimeter set on 1013 hPa will indicate approximately : | 6400 FT | 6800 FT | 6000 FT | 4000 FT | - | - | - | 0 |
| 4558 | 61 | Given : <br> ETA to cross a meridian is 2100 UTC GS is 441 kt <br> TAS is 491 kt | 75 kt | 60 kt | 40 kt | 90 kt | 0 | 0 | 1 | 0 |


| 4559 | 61 | The flight log gives the following data : <br> "True track, Drift, True heading, Magnetic variation, Magnetic heading, Compass deviation, Compass heading" <br> The right solution, in the same order, is : | $\begin{aligned} & 117^{\circ}, 4^{\circ} \mathrm{L}, \\ & 121^{\circ}, 1^{\circ} \mathrm{E}, \\ & 122^{\circ},-3^{\circ}, \\ & 119^{\circ} \end{aligned}$ | $\begin{aligned} & 125^{\circ}, 2^{\circ} \mathrm{R}, \\ & 123^{\circ}, 2^{\circ} \mathrm{W}, \\ & 121^{\circ},-4^{\circ}, \\ & 117^{\circ} \end{aligned}$ | $\begin{aligned} & 119^{\circ}, 3^{\circ}\llcorner, \\ & 122^{\circ}, 2^{\circ} \mathrm{E}, \\ & 120^{\circ},+4^{\circ}, \\ & 116^{\circ} \end{aligned}$ | $\begin{aligned} & 115^{\circ}, 5^{\circ} \mathrm{R}, \\ & 120^{\circ}, 3^{\circ} \mathrm{W}, \\ & 123^{\circ},+2^{\circ}, \\ & 121^{\circ} \end{aligned}$ | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4560 | 61 | Given : <br> Position 'A' N60 W020, <br> Position 'B' N60 W021, <br> Position 'C' N59 W020. | 52 NM and 60 NM | $60 \mathrm{NM} \text { and }$ $30 \text { NM }$ | $\begin{aligned} & 60 \mathrm{NM} \text { and } \\ & 52 \mathrm{NM} \end{aligned}$ | 30 NM and 60 NM | 0 | 0 |
| 4561 | 61 | Concerning direct reading magnetic compasses, in the northern hemisphere, it can be said that : | on an <br> Easterly heading, a Iongitudinal acceleration causes an apparent tum to the South | on a <br> Westerly hea ding, a Iongitudinal acceleration causes an apparent tum to the South | on a <br> Westerly hea ding, a Iongitudinal deceleration causes an apparent tum to the North | on an Easterly heading, a Iongitudinal acceleration causes an apparent tum to the North | 0 | 0 |
| 4562 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=225 \mathrm{kt}, \\ & \mathrm{HDG}\left({ }^{\circ} \mathrm{T}\right)=123^{\circ}, \end{aligned}$ | 134-178 kt | 134-188 kt | 120-190 kt | 128-180 kt | 1 | 0 |
| 4563 | 61 | Compass deviation is defined as the angle between: | True North and Compass North | the horizontal and the total intensity of the earth's magnetic field | Magnetic North and Compass North | True North and Magnetic Nor th | 0 | - |
| 4564 | 61 | At 0020 UTC an aircraft is crossing the $310^{\circ}$ radial at 40 NM of a VOR/DME station. <br> At 0035 UTC the radial is $040^{\circ}$ and DME distance is 40 NM . <br> Magnetic variation is zero. | 080 ${ }^{\circ}-226 \mathrm{kt}$ | 088 ${ }^{\circ}-232 \mathrm{kt}$ | 085 ${ }^{\circ}-226 \mathrm{kt}$ | 090 ${ }^{\circ}-232 \mathrm{kt}$ | 0 | 0 |
| 4565 | 61 | A straight line on a chart 4.89 cm long represents 185 NM . <br> The scale of this chart is approximately : | 1:5000 000 | 1:7000 000 | $1: 3500000$ | 1:6000 000 | 0 | 1 |
| 4566 | 61 | From the departure point, the distance to the point of equal time is : | inversely proportional to ground speed back | inversely proportional to the sum of ground speed out and ground speed back | proportional to the sum of ground speed out and ground speed back | inversely proportional to the total distance to go | - | 1-1 |
| 4567 | 61 | Given: <br> Required course $045^{\circ}(\mathrm{M})$; <br> Variation is $15^{\circ} \mathrm{E}$; <br> $\mathrm{W} / \mathrm{V}$ is $190^{\circ}(\mathrm{T}) / 30 \mathrm{kt}$; | $\begin{aligned} & 036^{\circ} \text { and } 151 \\ & \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 052^{\circ} \text { and } 154 \\ & \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 056^{\circ} \text { and } 137 \\ & \mathrm{kt} \end{aligned}$ | $\begin{aligned} & 055^{\circ} \text { and } 147 \\ & \mathrm{kt} \end{aligned}$ | - | - |
| 4568 | 61 | Given: $\text { TAS = } 270 \mathrm{kt} \text {, }$ <br> True HDG $=145^{\circ}$, | $6^{\circ} \mathrm{R}-259 \mathrm{kt}$ | $6^{\circ} \mathrm{L}-256 \mathrm{kt}$ | $6^{\circ} \mathrm{R}-251 \mathrm{kt}$ | $8^{\circ} \mathrm{R}-261 \mathrm{kt}$ | 0 | 1 |
| 4569 | 61 | Given: <br> Airport elevation is 1000 ft . <br> QNH is 988 hPa . <br> What is the approximate airport pressure altitude? | 1680 FT | 320 FT | 680 FT | - 320 FT | - | 0 |
| 4570 | 61 | Given: <br> Maximum allowable crosswind component is 20 kt . <br> Runway 06, RWY QDM $063^{\circ}(\mathrm{M})$. <br> Wind direction $100^{\circ}(\mathrm{M})$ | 25 kt | 33 kt | 31 kt | 26 kt | 0 | 1 |


| 4571 | 61 | The circumference of the parallel of latitude at $60^{\circ} \mathrm{N}$ is approximately: | 18706 NM | 20000 NM | \|34641 NM | 10800 NM | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4572 | 61 | Given: <br> Runway direction $230^{\circ}(\mathrm{T})$, | 31 kt | 36 kt | 21 kt | 26 kt | 1 | 0 | 0 | 0 |
| 4573 | 61 | Given: $\begin{aligned} & \text { True HDG = } 206^{\circ}, \\ & \text { TAS }=140 \mathrm{kt}, \\ & \text { Track }(\mathrm{T})=207^{\circ}, \end{aligned}$ | 180/10kt | 180/05kt | 000/05kt | 000/10kt | 0 | 1 | 0 | 0 |
| 4574 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=95 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=075^{\circ}, \end{aligned}$ | 8R-104 kt | 9R-108 kt | 10L - 104 kt | 9L-105 kt | 0 | 1 | 0 | 0 |
| 4575 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=227 \mathrm{kt}, \\ & \operatorname{Track}(\mathrm{~T})=316^{\circ}, \end{aligned}$ | 312-232 kt | 311 -230 kt | $313-235$ kt | 310-233 kt | 1 | 0 | 0 | 0 |
| 4576 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=198 \mathrm{kt}, \\ & \mathrm{HDG}\left({ }^{\circ} \mathrm{T}\right)=180, \end{aligned}$ | 179-220 kt | 181 -180 kt | $180-183 \mathrm{kt}$ | $180-223 \mathrm{kt}$ | 0 | 0 | 0 | 1 |
| 4577 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=200 \mathrm{kt}, \\ & \text { Track }(\mathrm{T})=073^{\circ}, \end{aligned}$ | 075-213 kt | 077-210 kt | 077-214 kt | 079-211 kt | - | 0 | 1-1 | 0 |
| 4578 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=200 \mathrm{kt}, \\ & \operatorname{Track}(\mathrm{~T})=110^{\circ}, \end{aligned}$ | 097-201 kt | 099-199 kt | 121 -207 kt | 121 -199 kt | 0 | 1 | 0 | 0 |
| 4579 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=270 \mathrm{kt}, \\ & \operatorname{Track}(\mathrm{~T})=260^{\circ}, \end{aligned}$ | 262-237 kt | 264-241 kt | 264-237 kt | 262-241 kt | 0 | 0 | - | 1 |
| 4580 | 61 | Given: $\begin{aligned} & \text { True HDG }=307^{\circ}, \\ & \text { TAS }=230 \mathrm{kt}, \\ & \text { Track }(\mathrm{T})=313^{\circ}, \end{aligned}$ | 265/30kt | 260/30kt | 257/35kt | 255/25kt | 0 | 1-1 | - | 0 |
| 4581 | 61 | $\begin{aligned} & \text { Given: } \\ & \text { True HDG }=233^{\circ}, \\ & \text { TAS }=480 \mathrm{kt}, \\ & \text { Track }(\mathrm{T})=240^{\circ}, \end{aligned}$ | 105/75kt | 110/75kt | 115/70kt | 110/80kt | 0 | 1 | - | 0 |
| 4582 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=155 \mathrm{kt}, \\ & \operatorname{Track}(\mathrm{~T})=305^{\circ}, \end{aligned}$ | 305-169 kt | 309-170 kt | 309-141 kt | 301-169 kt | 0 | 0 | 0 | 1 |
| 4583 | 61 | Given: $\begin{aligned} & \text { True HDG }=074^{\circ}, \\ & \text { TAS }=230 \mathrm{kt}, \\ & \text { Track }(\mathrm{T})=066^{\circ}, \end{aligned}$ | 180/40kt | 180/35kt | 180/30kt | 185/35kt | 0 | 1 | 0 | 0 |
| 4584 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=130 \mathrm{kt}, \\ & \operatorname{Track}(\mathrm{~T})=003^{\circ}, \end{aligned}$ | 002-173 kt | 359-166 kt | 357-168 kt | 001-170 kt |  | 0 | 0 | 1 |


| 4585 | 61 | \|Given: <br> True HDG $=054^{\circ}$, TAS $=450 \mathrm{kt}$, <br> Track $(T)=059^{\circ}$, | 010/45kt | 010/50kt | \|005/50kt | 010/55kt | 0 | 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4586 | 61 | $\begin{aligned} & \text { Given: } \\ & \text { True HDG }=145^{\circ}, \\ & \text { TAS }=240 \mathrm{kt}, \\ & \text { Track }(\mathrm{T})=150^{\circ}, \end{aligned}$ | 360/35kt | 180/35kt | 295/35kt | 115/35kt | 0 | 0 |  |
| 4587 | 61 | Given: True HDG = $002^{\circ}$, TAS = 130 kt, Track $(\mathrm{T})=353^{\circ}$, | 095/25kt | 095/20kt | 090/15kt | 090/20kt | 0 | 1 |  |
| 4588 | 61 | Given: <br> True HDG $=035^{\circ}$, <br> TAS $=245 \mathrm{kt}$, <br> Track $(T)=046^{\circ}$, | 335/55kt | 340/45kt | 340/50kt | 335/45kt | 0 | 0 | 0 |
| 4589 | 61 | Given: <br> course required $=085^{\circ}(T)$, <br> Forecast W/V 030/100kt, $\text { TAS }=470 \mathrm{kt},$ | 096, 29 MIN | 095, 31 MIN | 075 ${ }^{\circ}$, 39 MIN | $076{ }^{\circ}$, 34 MIN | 0 | 0 | 0 |
| 4590 | 61 | Given: <br> True course from A to $B=090^{\circ}$, $\begin{aligned} & \mathrm{TAS}=460 \mathrm{kt}, \\ & \mathrm{~W} / \mathrm{V}=360 / 100 \mathrm{kt}, \end{aligned}$ | 069 - 448 kt | 068 ${ }^{\circ}-460 \mathrm{kt}$ | 078 ${ }^{\circ}-450 \mathrm{kt}$ | 070 ${ }^{\circ}-453 \mathrm{kt}$ | 1 | - |  |
| 4591 | 61 | For a landing on runway $23\left(227^{\circ}\right.$ magnetic) surface W $/ \mathrm{V}$ reported by the ATIS is $180 / 30 \mathrm{kt}$. VAR is $13^{\circ} \mathrm{E}$. | 20 kt | 22 kt | 26 kt | 15 kt | 0 | 1 | - |
| 4592 | 61 | Given: <br> true track is $348^{\circ}$, <br> drift $17^{\circ}$ left, <br> variation $32^{\circ} \mathrm{W}$, | $033^{\circ}$ | $007^{\circ}$ | $359^{\circ}$ | $337^{\circ}$ | - | 0 | - |
| 4593 | 61 | Given: <br> Maximum allowable tailwind component for landing 10 kt . Planned runway 05 ( $047^{\circ}$ magnetic). <br> The direction of the surface wind reported by ATIS $210^{\circ}$. Variation is $17^{\circ} \mathrm{E}$. <br> Calculate the maximum allowable windspeed that can | 18 kt | 8 kt | 15 kt | 11 kt | 0 | 0 | 0 |
| 4594 | 61 | Given: True HDG = $133^{\circ}$, TAS = 225 kt, Track $(\mathrm{T})=144^{\circ}$, | 075/50kt | 075/45kt | 070/40kt | 070/45kt | 0 | 1 | 0 |
| 4595 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=190 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=355^{\circ}, \end{aligned}$ | 1R - 165 kt | 1L-215 kt | $1 \mathrm{~L}-225 \mathrm{kt}$ | 1R-175 kt | 0 | 1 | 0 |
| 4596 | 61 | Given: $\begin{aligned} & \text { TAS = } 140 \mathrm{kt}, \\ & \text { HDG }(T)=005^{\circ}, \end{aligned}$ | 11R - 142 kt | 11R - 140 kt | 10R - 146 kt | 9R-140 kt | 0 | 0 | 1-1 |


| 4597 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=465 \mathrm{kt}, \\ & \operatorname{Track}(\mathrm{~T})=007^{\circ}, \end{aligned}$ | \|358-428 kt | \|001-432 kt | $000-430 \mathrm{kt}$ | \|357-430 kt | 1 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4598 | 61 | Given: $\begin{aligned} & \text { TAS = } 485 \mathrm{kt}, \\ & \text { HDG }(T)=168^{\circ}, \end{aligned}$ | 175-420 kt | $175-432 \mathrm{kt}$ | $174-428 \mathrm{kt}$ | $173-424 \mathrm{kt}$ | 0 | 0 | 1 | 0 |
| 4599 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=230 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=250^{\circ}, \end{aligned}$ | 1L-225 kt | 1R-221 kt | 2R-223 kt | 2L-224 kt | 0 | 0 | 1 | 0 |
| 4600 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=90 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=355^{\circ}, \end{aligned}$ | 358-101 kt | 359-102 kt | 346-102 kt | 006-95 kt | 0 | 0 | 1 | - |
| 4601 | 61 | Given: $\begin{aligned} & \text { TAS = } 132 \mathrm{kt}, \\ & \text { HDG }(\mathrm{T})=053^{\circ}, \end{aligned}$ | 057-144 kt | 052-143 kt | 051-144 kt | 050-145 kt | 0 | 0 | 0 | 1 |
| 4602 | 61 | Given: $\begin{aligned} & \text { TAS = } 205 \mathrm{kt}, \\ & \text { HDG }(T)=180^{\circ}, \end{aligned}$ | 4L - 195 kt | 6L-194 kt | 7L - 192 kt | 3L-190 kt | 0 | - | 0 | 0 |
| 4603 | 61 | Given: $\begin{aligned} & \mathrm{TAS}=250 \mathrm{kt}, \\ & \mathrm{HDG}(\mathrm{~T})=029^{\circ}, \end{aligned}$ | 1L-205 kt | 1R-205 kt | 1L - 265 kt | 1R-295 kt | 1 | 0 | 0 | 0 |

